

# Inverse Volume Rendering with Material Dictionaries: Supplementary Material

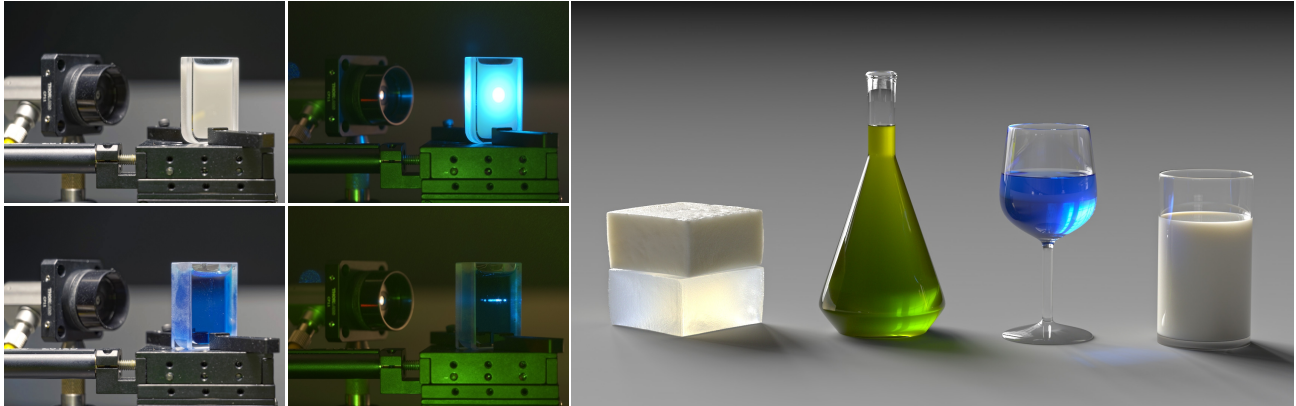
Ioannis Gkioulekas  
Harvard University

Shuang Zhao  
Cornell University

Kavita Bala  
Cornell University

Todd Zickler  
Harvard University

Anat Levin  
Weizmann Institute



**Figure 1:** Acquiring scattering parameters. Left: Samples of two materials (milk, blue curacao) in glass cells used for acquisition. Middle: Samples illuminated by a trichromatic laser beam. The observed scattering pattern is used as input for our optimization. Right: Rendering of materials in natural illumination using our acquired material parameter values.

## Abstract

Translucent materials are ubiquitous, and simulating their appearance requires accurate physical parameters. However, physically-accurate parameters for scattering materials are difficult to acquire. We introduce an optimization framework for measuring bulk scattering properties of homogeneous materials (phase function, scattering coefficient, and absorption coefficient) that is more accurate, and more applicable to a broad range of materials. The optimization combines stochastic gradient descent with Monte Carlo rendering and a material dictionary to invert the radiative transfer equation. It offers several advantages: (1) it does not require isolating single-scattering events; (2) it allows measuring solids and liquids that are hard to dilute; (3) it returns parameters in physically-meaningful units; and (4) it does not restrict the shape of the phase function using Henyey-Greenstein or any other low-parameter model. We evaluate our approach by creating an acquisition setup that collects images of a material slab under narrow-beam RGB illumination. We validate results by measuring prescribed nano-dispersions and showing that recovered parameters match those predicted by Lorenz-Mie theory. We also provide a table of RGB scattering parameters for some common liquids and solids, which are validated by simulating color images in novel geometric configurations that match the corresponding photographs with less than 5% error.

**CR Categories:** I.3.7 [Computer Graphics]: Three-Dimensional Graphics and Realism—Raytracing;

**Keywords:** scattering, inverse rendering, material dictionaries

**Links:** [DL](#) [PDF](#) [WEB](#)

## 1 Introduction

Scattering plays a critical role in the appearance of most materials. Much effort has been devoted to modeling and simulating its visual effects, giving us precise and efficient scattering simulation algorithms. However, these algorithms produce images that are only as accurate as the material parameters given as input. This creates a need for acquisition systems that can faithfully measure the scattering parameters of real-world materials.

Collecting accurate and repeatable measurements of scattering is a significant challenge. For homogeneous materials—which is the primary topic of this paper—scattering at any particular wavelength is described by two scalar values and one angular function. The *scattering coefficient*  $\sigma_s$  and *absorption coefficient*  $\sigma_a$  represent the fractions of light that are scattered and absorbed, and the *phase function*  $p(\theta)$  describes the angular distribution of scattering. Measurement is difficult because a sensor almost always observes the combined effects of many scattering and absorption events, and these three factors cannot be easily separated. Indeed, for deeply-scattering geometries, similarity theory [Wyman et al. 1989] proves that one can analytically derive distinct parameter-sets that nonetheless produce indistinguishable images.

Most existing acquisition systems address the measurement challenge using a combination of two strategies (e.g., [Hawkins et al. 2005; Narasimhan et al. 2006; Mukaigawa et al. 2010]). First, they manipulate lighting and/or materials to isolate single-scattering effects; and second, they “regularize” the recovered scattering parameters by relying on a low-parameter phase function model, such as the Henyey-Greenstein (HG) model. These approaches can provide accurate results, but both of the employed strategies have severe limitations. The single-parameter HG model limits applicability to materials that it represents well; and this excludes some common natural materials [Gkioulekas et al. 2013]. Meanwhile, isolating single scattering relies on either: (a) diluting the sample [Hawkins et al. 2005; Narasimhan et al. 2006], which cannot be easily applied to solids or to liquids that have unknown dispersing media; or, (b) using structured lighting patterns [Mukaigawa et al. 2010], which provide only approximate isolation [Holroyd and Lawrence 2011; Gupta et al. 2011] and therefore induce errors in measured scattering parameters that are difficult to characterize.

We introduce an optimization framework that allows measuring homogeneous scattering parameters without these limitations. Our optimization undoes the effects of low-order scattering by inverting the radiative transfer equation (i.e., by inverting a random walk) using a combination of Monte Carlo rendering and stochastic gradient descent. We evaluate our optimization framework by creating a volumetric scanner that uses a camera and narrow-beam RGB sources to collect a handful of images of a material sample that resides in a box-shaped transparent glass cell (Figure 1, left). Once calibrated, this scanner provides images of low-order scattering in which the geometry is precisely known. Using these images we optimize a dictionary-based set of scattering parameters so that they produce re-rendered images that match the acquired ones.

We validate our results in two ways: one, we measure prescribed dispersions of nano-scale particles whose scattering parameters can be computed using Lorenz-Mie theory and show that our recovered parameters are in close agreement; two, we re-render color images of these materials in novel lighting configurations and show that they numerically match, within 5%, the new captured images.

The benefits of our approach are:

(1) We can accurately measure scattering for a broader set of liquids *and* solids since there is no need for precisely-isolated single-scattering effects. The thickness of the glass cell can be selected appropriately for each material; but it does not need to be chosen with excessive care since our optimization succeeds for a relatively broad range of thicknesses (anywhere between 0.1 to 10 times the mean free path of the material being measured).

(2) We can support general phase function measurement, and are not restricted to HG or other low parameter models, because our optimization incorporates a large material dictionary that allows phase functions to be any convex combination of hundreds of dictionary elements. These general phase functions are particularly visually important for accurate visual appearance of objects with thin features.

Our contributions include:

- An optimization framework to invert volumetric scattering using MC rendering and stochastic gradient descent.
- An acquisition setup to acquire homogeneous material scattering properties with physically accurate parameters.
- A table of RGB scattering parameters for a variety of common materials, both liquid and solid, as well as a publicly-available collection of tabulated phase functions.

The availability of physically-accurate scattering parameters with general phase functions can improve simulations of translucent material appearance to better match that in the real world.

## 2 Related Work

Inverse radiative transport is studied in graphics, as well as in geophysical, biomedical, and chemistry domains; Bal [2009] provides a comprehensive review. Problems can be grouped into three categories, according to the ratio of the material’s mean free path—the average distance a photon travels before it is scattered—to the size of the scattering volume. We discuss these three categories in turn, and then we discuss phase function models and surface-based appearance models.

**Deep scattering and approximation by diffusion.** Inverse problems in this category consider media that are optically-thick, so that photons scatter many times before being measured. Radiative transport is then modeled using the diffusion approximation, where the angular variation of the internal radiance is limited and the radiative

transport equation reduces to a partial differential equation [Ishimaru 1978]. The advantage of this approach is that it simplifies the inference problem, allowing efficient acquisition and rendering systems [Jensen et al. 2001; Donner and Jensen 2005] and, as demonstrated by Wang et al. [2008], the estimation of spatially-varying structure within a medium. In physics, the diffusion approximation is employed by diffusing-wave spectroscopy [Pine et al. 1990], which is used for applications such as particle sizing or the measurement of molecular weight. The diffusion approximation applies when high-order scattering is dominant, causing the phase function to be confounded with other scattering parameters [Wyman et al. 1989] and therefore reasonable to ignore. It is not appropriate for our application, where we seek material-specific phase functions that can accurately predict appearance for shapes that have arbitrary thin and thick parts.

**Single scattering and direct methods.** At the other extreme are optically-thin situations, where photons scatter only once before being measured. Scattering parameters can often be measured directly in these cases, using techniques like static or dynamic light scattering [Johnson and Gabriel 1994]. For graphics, Hullin et al. [2008] use fluorescent dyes to make qualitative observations on the scattering parameters of optically thin media exhibiting mostly single scattering. Hawkins et al. [2005] use a laser to measure albedo and a tabulated phase function of a sparse homogeneous aerosol. For liquids, Narasimhan et al. [2006] successively dilute samples with water until they are sparse enough to infer from single-scattering an HG phase function. Single-scattering has also been exploited to capture time-varying and spatially-varying wisps of smoke and sparse mixing liquids [Hawkins et al. 2005; Fuchs et al. 2007; Gu et al. 2008]. All of these techniques rely on manipulating materials so that single-scattering dominates, and while dilution can be used for aerosols and some liquids, it cannot be easily applied to solids, or to liquids whose dispersing medium is unknown and significantly different from water. This limitation motivates methods for suppressing multiple scattering without dilution. Techniques for particle sizing or molecular weight, for example, exploit cross-correlation properties of multiple temporal measurements [Pusey 1999], but these are specific to those applications and do not easily extend to our problem. For graphics, Mukaigawa et al. [2010] use high frequency lighting patterns to isolate single-scattering effects [Nayar et al. 2006], allowing direct access to the mean free path and a good initialization for an indirect (multi-scattering) optimization over an HG phase function parameter. Such lighting-based isolations of single scattering are potentially quite useful, but as discussed in the context of 3D surface reconstruction [Holroyd and Lawrence 2011; Gupta et al. 2011], they provide only approximate isolation, and there is currently no analysis of how this affects the accuracy of inferred scattering parameters.

**Low-order scattering and indirect methods.** Our approach is in this category, where the goal is use moderately-thick samples to infer scattering parameters by iteratively refining them until they predict measurements that are consistent with the acquired ones (e.g., [Singer et al. 1990; Mukaigawa et al. 2010]). Most of these approaches focus like we do on homogeneous materials, since this is already very challenging. (A notable exception is Antyufeev [2000], who used regularized estimation to infer spatially-varying phase functions.) A common strategy in biomedical and physics domains is to simplify calculations by using planar slabs and spatially-uniform lighting that reduces the relevant scene geometry from three dimensions to two (e.g., [Chen et al. 2006; Prah et al. 1993; McCormick and Sanchez 1981]). But this has the significant disadvantage of limiting access to angular scattering information, thereby increasing reliance on restrictive low-parameter phase function models. In contrast, our optimization applies to any geometrical configuration with any incident light field, as long as both

are precisely calibrated. This allows using narrow-beam illumination, which improves access to angular scattering information and allows considering a much richer space of phase function models.

**Phase function models.** Most existing approaches to inverse radiative transfer use the single parameter Henyey-Greenstein [1941] model or other low-parameter models [Reynolds and McCormick 1980], but these can only be accurate for materials they represent well. The shape of the phase function is important for appearance, especially for objects with thin parts, and as recently shown by Gkioulekas et al. [2013], there are common materials that are not well-represented by the HG model. We avoid the restrictions of low-parameter models through the use of a phase function dictionary with hundreds of elements. This is similar in spirit to dictionary-based BRDF representations used to analyze and edit opaque scenes without being restricted to any particular analytic BRDF model (e.g., [Lawrence et al. 2006; Ben-Artzi et al. 2008]).

**Surface reflectance fields and BSSRDF.** There are a number of acquisition systems devoted to recovering surface-based descriptions of light transport through translucent objects [Debevec et al. 2000; Goesele et al. 2004; Tong et al. 2005; Peers et al. 2006; Donner et al. 2008]. These provide mappings between the input and output light fields on a specific object’s surface, and they do so without explicitly estimating all of the internal scattering parameters. They have the advantage of being very general and providing accurate appearance models for heterogeneous objects with complex shapes. Our goal is very different. We seek scattering material parameters that are independent of geometry, so that we can easily edit these materials and accurately predict their appearance when sculpted into *any* geometric shape.

### 3 Volume light transport

Scattering occurs as light propagates through a medium and interacts with material structures. There are many *volume events* that cause absorption or change of propagation direction. This process has been modeled by the *radiative transfer equation* (RTE) [Chandrasekhar 1960; Ishimaru 1978]:

$$\begin{aligned} (\boldsymbol{\omega}^T \nabla) L(\mathbf{x}, \boldsymbol{\omega}) &= Q(\mathbf{x}, \boldsymbol{\omega}) - \sigma_t L(\mathbf{x}, \boldsymbol{\omega}) \\ &+ \sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\omega}, \boldsymbol{\psi}) L(\mathbf{x}, \boldsymbol{\psi}) \, d\mu(\boldsymbol{\psi}), \end{aligned} \quad (1)$$

where  $\mathbf{x} \in \mathbb{R}^3$  is a point in the interior or boundary of the scattering medium;  $\boldsymbol{\omega}, \boldsymbol{\psi} \in \mathbb{S}^2$  are points in the sphere of directions and  $\mu$  is the usual spherical measure;  $Q(\mathbf{x}, \boldsymbol{\omega})$  accounts for emission from light sources; and  $L(\mathbf{x}, \boldsymbol{\omega})$  is the resulting light field radiance at every spatial location and orientation. The material is characterized by the triplet of macroscopic bulk parameters  $k = \{\sigma_t, \sigma_s, p(\theta)\}$ . Specifically, the *extinction coefficient*  $\sigma_t$  controls the spatial frequency of scattering events, and the *scattering coefficient*  $\sigma_s \leq \sigma_t$  the amount of light that is scattered. The difference  $\sigma_a = \sigma_t - \sigma_s \geq 0$  is known as the *absorption coefficient* and is the amount of light that is absorbed. Finally, the *phase function*  $p$  is a function on  $\mathbb{S}^2 \times \mathbb{S}^2$  determining the amount of light that gets scattered towards each direction  $\boldsymbol{\psi}$  relative to the incident direction  $\boldsymbol{\omega}$ . The phase function is often assumed to be invariant to rotations of the incident direction and cylindrically symmetric; therefore, it is a function of only  $\theta = \arccos(\boldsymbol{\omega} \cdot \boldsymbol{\psi})$  satisfying the normalization constraint

$$2\pi \int_{\theta=0}^{\pi} p(\theta) \sin(\theta) \, d\theta = 1. \quad (2)$$

We also adopt this assumption in the remaining of the paper and consider only phase functions of this type (we discuss some of the technical details related to this assumption in Appendix C). Complementary to the above quantities, the following two parameters

are also used for describing scattering behavior: the *mean free path*, equal to  $d = 1/\sigma_t$ , and the *albedo*, equal to  $a = \sigma_s/\sigma_t$ . In the following, we will use the parameter triplet  $k$  as an interchangeable term for scattering material.

We consider homogeneous materials in which scattering parameters do not depend on spatial location. Scattering parameters also exhibit perceptually dominant spectral dependency [Fleming and Bülthoff 2005; Frisvad et al. 2007] but for notational clarity we omit wavelength dependency.

#### 3.1 Operator-theoretic formulation

We present the operator-theoretic formulation of the RTE that we will use to setup a tractable optimization procedure for volume rendering inversion. The specific formulation we use is tailored toward our optimization algorithm, but approximations of similar nature have been considered for rendering applications [Rushmeier and Torrance 1987; Bhate and Tokuta 1992]. In the following, we consider only points  $\mathbf{x}$  in the interior of the scattering medium; we discuss boundary conditions and other details for this formulation in Appendix A.

We begin by considering a finite difference approximation for the directional derivative [LeVeque 2007]

$$(\boldsymbol{\omega}^T \nabla) L(\mathbf{x}, \boldsymbol{\omega}) \approx \frac{1}{h} (L(\mathbf{x} + h\boldsymbol{\omega}, \boldsymbol{\omega}) - L(\mathbf{x}, \boldsymbol{\omega})). \quad (3)$$

Defining  $L_i(\mathbf{x}, \boldsymbol{\omega}) = hQ(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\omega})$ , after simple algebraic manipulation we obtain from Equation (1)

$$\begin{aligned} L(\mathbf{x}, \boldsymbol{\omega}) &= L_i(\mathbf{x}, \boldsymbol{\omega}) + (1 - h\sigma_t) L(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\omega}) + \\ &h\sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\omega}^T \boldsymbol{\psi}) L(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\psi}) \, d\mu(\boldsymbol{\psi}). \end{aligned} \quad (4)$$

We define the following linear operator in terms of the material parameters  $k = \{\sigma_t, \sigma_s, p(\theta)\}$ , that acts on functions on  $\mathbb{R}^3 \times \mathbb{S}^2$

$$\begin{aligned} \mathcal{K}_k(L)(\mathbf{x}, \boldsymbol{\omega}) &\triangleq (1 - h\sigma_t) L(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\omega}) \\ &+ h\sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\omega}^T \boldsymbol{\psi}) L(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\psi}) \, d\mu(\boldsymbol{\psi}). \end{aligned} \quad (5)$$

Intuitively, the action of  $\mathcal{K}_k$  can be viewed as a single step in the temporal propagation of a photon inside the medium. After traveling a distance of length  $h$ , the photon will transit in one of the following ways: 1) keep the same direction unaffected by the medium (probability  $1 - h\sigma_t$ ); 2) scatter towards a new direction determined by the phase function  $p$  (probability  $h\sigma_s$ ); 3) absorbed (probability  $h(\sigma_t - \sigma_s)$ ). Consecutive applications of  $\mathcal{K}_k$  describe the time-resolved random walk the photon performs as it travels through the medium.

Using the  $\mathcal{K}_k$  operator, we can rewrite the RTE (4) in the form

$$L = L_i + \mathcal{K}_k L. \quad (6)$$

Solving Equation (6) for  $L$ , we can express the light field  $L$  as the result of a radiative transfer process  $\mathcal{R}_k$  on the input light field  $L_i$ :

$$L = \mathcal{R}_k L_i, \quad (7)$$

with

$$\mathcal{R}_k \triangleq (\mathcal{I} - \mathcal{K}_k)^{-1} = \sum_{j=0}^{\infty} \mathcal{K}_k^j. \quad (8)$$

The second equality in Equation (8) follows by applying the Neumann series expansion, as it applies for the inverse of  $\mathcal{I} - \mathcal{K}_k$ . (We

discuss the invertibility of  $\mathcal{I} - \mathcal{K}_k$  in Appendix C.) It implies that the light field  $L$  resulting from the radiative transfer process of Equation (3) can be expressed as the sum of all orders of consecutive applications  $\mathcal{K}_k$  to the input light field  $L_i$ . That is,  $L$  corresponds to the asymptotic density of photons, when accounting for all of the intermediate positions of each photon after an arbitrary number of random walk steps. We refer to  $\mathcal{K}_k$  as the *single-step propagation operator* and to  $\mathcal{R}_k$  as the *rendering operator* for material  $k$ .

The validity of the above formulation for volume light transport relies on the accuracy of the approximation in Equation (3). In the limit that  $h$  goes to zero, the operator  $\mathcal{R}_k$  and the light field  $L$  of Equation (7) converge to the usual *volume rendering operator* [Jensen 2001] and the true light field inside the volume. In Appendix A, we discuss in detail this relationship, as well as analogies between operator  $\mathcal{K}_k$  and Equation (8), and their counterparts derived from the volume rendering equation. As explained there, how small  $h$  needs to be depends on the extinction coefficient  $\sigma_t$  of the medium:  $h \ll \varepsilon/\sigma_t$ . In our experiments, we use  $\varepsilon = 0.01$ .

## 4 Inverting volume scattering

We are interested in using images of an unknown material, to recover its scattering parameters  $k = \{\sigma_t, \sigma_s, p(\theta)\}$ . Formally, we consider a known 3D shape filled with the unknown material, illuminated by calibrated light sources  $L_i^m$ , and imaged by calibrated cameras to produce images  $I^m$ . Using the volume scattering Equation (6), we can write

$$I^m = \mathcal{S}^m L = \mathcal{S}^m (\mathcal{I} - \mathcal{K}_k)^{-1} L_i^m, \quad (9)$$

where the sampling operator  $\mathcal{S}^m$  describes the combination of light field rays measured by the corresponding camera. The terms  $L_i^m$  and  $\mathcal{S}^m$  fold in complete information about the 3D shape of the material volume, the relative light source and camera positions, as well as light interactions at the interface between the material volume and its surroundings. Modeling these light interactions involves a knowledge of the materials' refractive indices, and an assumption there is no further scattering between the material and the camera.

Given a set of illuminations  $\{L_i^m, m = 1, \dots, M\}$  and their corresponding measurements  $\{I^m, m = 1, \dots, M\}$ , we cast the problem of inferring the material properties in an *appearance matching* framework: find the material parameters  $k$  that best reproduce the measurements in the least-squares sense

$$\min_k \sum_{m=1}^M w_m (\mathcal{S}^m (\mathcal{I} - \mathcal{K}_k)^{-1} L_i^m - I^m)^2. \quad (10)$$

where  $k$  is any permissible material parameter triplet  $\{\sigma_t, \sigma_s, p(\theta)\}$ . We weight the error for each radiance measurement with  $w_m = \max\{c, (\bar{I}^m)^\alpha\}^{-1}$ ,  $c, \alpha > 0$ , to prevent the solution from overfitting only the brightest measurements. We selected  $c = 0.01$  and  $\alpha = 3$  using the experiments on synthetic data described in Section 6.

In the rest of this section we derive an optimization algorithm for the appearance matching problem. We express the material parameters as a convex linear combination of the material dictionary. We then differentiate the appearance matching error with respect to the mixing weights and derive an efficient optimization scheme based on stochastic gradient descent and Monte-Carlo rendering. Despite the highly non-linear problem, we show through simulations that the error surface is smooth without local minima and allows accurate reconstruction of material parameters.

### 4.1 Dictionary representation of materials

To better parameterize the search space in Equation (10), we use a *dictionary representation* for the materials. Specifically, consider a dictionary set of materials  $D = \{k_n, n = 1, \dots, N\}$ , where  $k_n = \{\sigma_{t,n}, \sigma_{s,n}, p_n(\theta)\}$ , and their corresponding single-step propagation operators  $\{\mathcal{K}_{k_n}\}$ . Then, for any weight vector  $\pi$  in the  $N$ -dimensional simplex  $\Delta^N$ ,

$$\pi = [\pi_n] \in \mathbb{R}^N, \pi_n \geq 0, n = 1, \dots, N, \sum_{n=1}^N \pi_n = 1, \quad (11)$$

we can represent a novel *mixture material*  $k(\pi) = \{\sigma_{t,\pi}, \sigma_{s,\pi}, p_\pi(\theta)\}$ , in terms of the dictionary atoms as:

$$\sigma_{t,\pi} \triangleq \sum_{n=1}^N \pi_n \sigma_{t,n}, \quad \sigma_{s,\pi} \triangleq \sum_{n=1}^N \pi_n \sigma_{s,n}, \quad (12)$$

$$p_\pi(\theta) \triangleq \frac{\sum_{n=1}^N \pi_n \sigma_{s,n} p_n(\theta)}{\sum_{n=1}^N \pi_n \sigma_{s,n}}. \quad (13)$$

It is easy to see that if each  $p_n(\theta)$  satisfies the normalization condition of Equation (2), so does  $p_\pi(\theta)$ .

In the following, we denote by  $\mathcal{K}(\pi)$  and  $\mathcal{R}(\pi)$  the single-step propagation (Equation (5)) and rendering (Equation (8)) operators, respectively, for the material  $k(\pi)$ . We denote the appearance matching error of the mixing weights  $\pi$  as

$$E(\pi) = \sum_{m=1}^M w_m (\mathcal{S}^m (\mathcal{I} - \mathcal{K}(\pi))^{-1} L_i^m - I^m)^2. \quad (14)$$

Then, we search for a convex combination of the material atoms in the dictionary  $D$  which best reproduces the captured images, by minimizing  $E(\pi)$  over  $\pi \in \Delta^N$ .

To justify our use of convex combinations  $\pi$  and the mixing Equations (12)-(13), we present the following lemma.

**Lemma 1.** *For any vector  $\pi \in \Delta^N$ , the single-step propagation operator  $\mathcal{K}(\pi)$  for the mixed material  $k(\pi)$  defined by Equations (12)-(13), is a convex combination of the single-step propagation operators of the individual atoms, with the exact same mixing weights,*

$$\mathcal{K}(\pi) = \sum_{n=1}^N \pi_n \mathcal{K}_{k_n}. \quad (15)$$

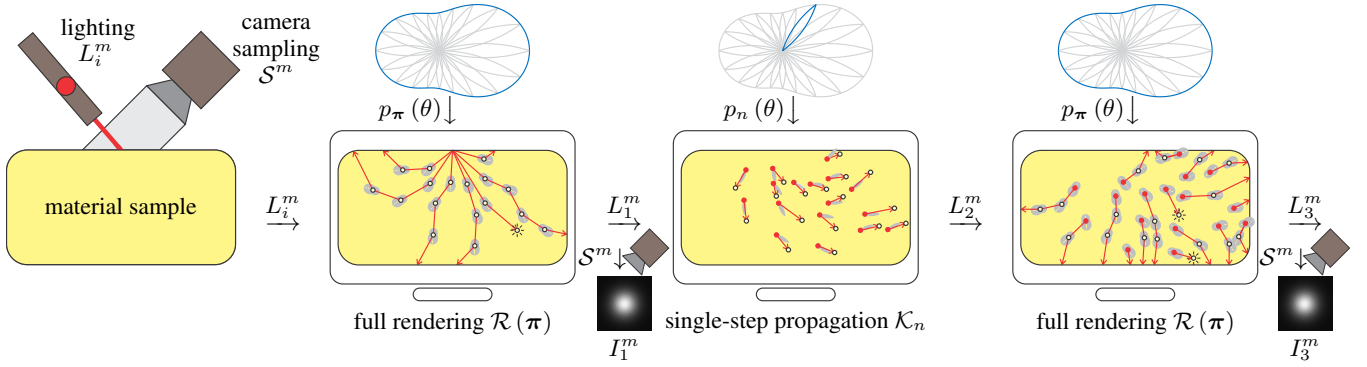
*Proof.* Denoting  $f = L(\mathbf{x} - h\boldsymbol{\omega}, \boldsymbol{\omega})$ , and using Equation (5),

$$\begin{aligned} \sum_{n=1}^N \pi_n \mathcal{K}_{k_n}(L) &\stackrel{(5)}{=} \underbrace{\left(\sum_{n=1}^N \pi_n - h \left(\sum_{n=1}^N \pi_n \sigma_{t,n}\right)\right)}_{=1} f \\ &+ h \int_{\mathbb{S}^2} \left(\sum_{n=1}^N \pi_n \sigma_{s,n} p_n(\boldsymbol{\omega}^T \boldsymbol{\psi})\right) f(\mathbf{x}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}). \end{aligned} \quad (16)$$

For the expression of Equation (16) to be an operator of the form of Equation (5), we express the integral as:

$$\underbrace{\left(\sum_{n=1}^N \pi_n \sigma_{s,n}\right)}_{\triangleq \sigma_{s,\pi}} \int_{\mathbb{S}^2} \underbrace{\left(\frac{\sum_{n=1}^N \pi_n \sigma_{s,n} p_n(\boldsymbol{\omega}^T \boldsymbol{\psi})}{\sum_{n=1}^N \pi_n \sigma_{s,n}}\right)}_{\triangleq p_\pi(\theta)} f(\mathbf{x}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}). \quad (17)$$

From Equations (16) and (17), we get exactly the single-step propagation operator of the material  $k(\pi)$  in Equation (15).  $\square$



**Figure 2:** Gradient computation (Equation (19)) for the dictionary-based appearance matching optimization problem (Equation (14)). For each pair of lighting and viewing directions, the gradient with respect to the weight of the  $n$ -th dictionary material requires computing a cascade of three rendering operations: a full volume rendering using the mixture material; then a single-step propagation using the corresponding atom material; then another full volume rendering using the mixture material. The resulting light fields are then sampled to produce the images used algebraically in Equation (19).

Lemma 1 shows that a convex combination of materials  $k_n$  can be directly identified with a convex combination of single-step propagation operators  $\mathcal{K}_{k_n}$ . As a result, the objective function of the optimization problem of Equation (14) has a much simpler functional dependence on the parameters  $\pi$  we optimize over, allowing us to derive a tractable optimization strategy as discussed in the following subsection. This property is the key motivator for our use of the finite-difference approximation in the operator-theoretic formulation of Section 3.1. As shown in Appendix A deriving an analogous result from a volume rendering formulation, in contrast, requires that the extinction coefficient be known beforehand and fixed for all the atoms in dictionary  $D$ .

## 4.2 Optimization Algorithm

To minimize the appearance matching error of Equation (14), we differentiate it with respect to the mixing weights  $\pi$  using the following lemma:

**Lemma 2.** For the operator  $\mathcal{K}(\pi)$  defined in Equation (15), the following differentiation rule holds

$$\frac{\partial}{\partial \pi_n} (\mathcal{I} - \mathcal{K}(\pi))^{-1} = (\mathcal{I} - \mathcal{K}(\pi)) \mathcal{K}_{k_n} (\mathcal{I} - \mathcal{K}(\pi)). \quad (18)$$

This is a well-known result in the case of finite-dimensional matrices. In Appendix C, we provide a precise statement and proof of the lemma for the case of infinite-dimensional linear operators.

Using Equations (15) and (18), we can write the gradient of  $E(\pi)$  with respect to each coordinate of the mixture weight vector  $\pi$  as

$$\begin{aligned} \frac{\partial E}{\partial \pi_n}(\pi) &= \sum_{m=1}^M 2w_m \left( \mathcal{S}^m \left( \underbrace{(\mathcal{I} - \mathcal{K}(\pi))^{-1} L_i^m}_{\triangleq L_1^m} - \bar{I}^m \right) \right. \\ &\quad \cdot \underbrace{\mathcal{S}^m \left( (\mathcal{I} - \mathcal{K}(\pi))^{-1} \mathcal{K}_{k_n} \left( \underbrace{(\mathcal{I} - \mathcal{K}(\pi))^{-1} L_i^m}_{\triangleq L_1^m} \right)}_{\triangleq L_2^m} \right)}_{\triangleq L_3^m} \left. \right). \end{aligned} \quad (19)$$

Equation (19) is crucial for our optimization. It shows that the gradient computation simplifies to rendering and sampling operations:

1. Render a light field  $L_1^m$  starting from input radiance  $L_i^m$ , and using the rendering operator  $\mathcal{R}(\pi)$ .
2. Apply the single-step propagation operator  $\mathcal{K}_{k_n}$ , corresponding to the  $n$ -th material  $k_n$  in the dictionary  $D$ , on  $L_1^m$ , producing a light field  $L_2^m$ .
3. Render a light field  $L_3^m$ , by applying the full rendering operator  $\mathcal{R}(\pi)$  on  $L_2^m$ .
4. Apply the sampling operator  $\mathcal{S}^m$  on  $L_1^m$  and  $L_3^m$ , and evaluate their product (Equation (19)).

These gradient evaluation steps are summarized in Algorithm 1, and visualized in Figure 2.

**Rendering.** The fact that the appearance error gradient can be expressed as a sequence of rendering steps has an important practical implication: it allows us to evaluate it efficiently using Monte-Carlo rendering techniques [Dutr e et al. 2006]. For the first stage, in our implementation we use the traditional volume rendering operator (described in Appendix A), as for small enough  $h$  it produces equivalent results to the rendering operator  $\mathcal{R}(\pi)$  of our finite-difference formulation. We estimate separately the direct illumination term (which depends only on the assumed known radiance sources in the scene and is easy to compute) and the indirect component. For the latter, we use a Monte-Carlo particle tracing process to estimate  $I_1$ , while simultaneously caching all intermediate particle positions in a set  $C_1$  to form an approximation of  $L_1$ . This process is described in Algorithm 3. Then the application of  $\mathcal{K}_k$  on  $L_1$  is stochastically approximated as described in Algorithm 4: particles are uniformly sampled from  $C_1$ , propagated by  $h$ , and then either scattered or absorbed. The results are cached in a set  $C_2$  as an approximation of  $L_2$ . Finally, samples from  $C_2$  are used as sources for another full particle tracing process that directly estimates  $I_3$ , without further caching. This is performed similar to Algorithm 3, but with the initialization of  $\mathbf{x}$  and  $\omega$  in Step 2 replaced by an initialization from a particle drawn uniformly from  $C_2$  and with the caching Step 10 omitted. We discuss further details about the algorithm we use to render  $\frac{\partial E}{\partial \pi_n}$ , including handling of Fresnel reflection and refraction, in Appendix B.

**Stochastic gradient descent.** The availability of stochastic estimates of the gradient makes *stochastic gradient descent* (SGD) algorithms attractive for minimizing Equation (14). Similar to standard gradient descent, SGD algorithms perform iterations of steps

---

**Algorithm 1** ComputeGradient.
 

---

**Input:**  $\pi \in \Delta^N$ .  
 1: **for**  $n = 1$  to  $N$  **do**  
 2:    $g_n \leftarrow 0$ .  
 3:   **for**  $m = 1$  to  $M$  **do**  
 4:     Render  $L_1^m \leftarrow \mathcal{R}(\pi) L_i^m$ .  
 5:     Apply single-step propagation  $L_2^m \leftarrow \mathcal{K}_{k_n} L_1^m$ .  
 6:     Render  $L_3^m \leftarrow \mathcal{R}(\pi) L_2^m$ .  
 7:     Sample  $I_1^m \leftarrow \mathcal{S}^m L_1^m$ .  
 8:     Sample  $I_3^m \leftarrow \mathcal{S}^m L_3^m$ .  
 9:      $g_n \leftarrow g_n + 2w_m (I_1^m - \bar{I}^m) I_3^m$ .  
 10:   **end for**  
 11: **end for**  
 12: **return**  $g$ .

---

proportional to the negative of the stochastic estimates of the gradient. These algorithms only require that the estimates be unbiased; even if they are otherwise noisy, there exist convergence guarantees analogous to those of standard gradient descent, with the noise variance only affecting convergence speed. This behavior has an important practical implication: we can reduce the number of particles in Monte-Carlo evaluations of the gradient, and speed computation at the cost of introducing noise to the gradient estimate. As long as the rendering algorithm is unbiased such noisy gradient estimates are valid inputs to SGD. The noise due to the reduced number of particles somewhat increases the number of iterations. However, it is still possible to reduce the number of particles quite drastically, and achieve a significant speedup in terms of overall computation time [Bottou and Bousquet 2008].

As the vector  $\pi$  is constrained to lie on the simplex, we use *projected stochastic gradient descent* (PSGD). We denote by  $g \in \mathbb{R}^N$  consecutive noisy estimates of the gradient of  $E(\pi)$  obtained through Monte-Carlo rendering such that

$$\mathbb{E}[g_n] = \frac{\partial E(\pi)}{\partial \pi_n}. \quad (20)$$

We use them to iterate

$$\pi^{(t+1)} = \mathcal{P}_{\Delta^N} \left( \pi^{(t)} - \eta^{(t)} g^{(t)} \right), \quad (21)$$

where  $\mathcal{P}_{\Delta^N}$  denotes the Euclidean projection operator to the simplex  $\Delta^N$  [Duchi et al. 2008]. The step size is often chosen equal to  $\eta^{(t)} = \frac{c}{\sqrt{t}}$ . Though the speed of convergence depends on the proportionality constant  $c$ , in practice SGD is known to be robust to this selection. To cancel noise in individual steps, SGD returns as its final output the average of all  $T$  iterations,  $\pi^{\text{opt}} = \frac{1}{T} \sum_{t=0}^T \pi^{(t)}$ . This procedure is summarized in Algorithm 2.

The optimization problem we solve is highly non-linear and essentially involves inversion of the photon random walk process. Despite the non-linear formulation, our simulations in Section 6.2 show it allows an accurate reconstruction of material parameters. While an exact proof of this property is a subject for further research, all our simulations indicate that the error surface is very smooth and does not suffer from local minima, explaining the good convergence we are able to achieve.

### 4.3 Dictionary

The dictionary-based formulation of the appearance matching problem in Equation (14) can be used with any dictionary choice<sup>1</sup>. Our own simple dictionary is described below. We start with the phase

<sup>1</sup>We use the term ‘‘dictionary’’ because the phase function sets we use can be under- or over-complete and not strictly ‘‘bases’’ in the technical sense.

---

**Algorithm 2** Solve appearance matching optimization problem.
 

---

1: Initialize  $\pi_n^{(0)} \leftarrow 1/N$ .  
 2: **while** not converged **do**  
 3:    $g^{(t)} \leftarrow \text{ComputeGradient}(\pi^{(t)})$ .  
 4:    $\pi^{(t+1)} \leftarrow \mathcal{P}_{\Delta^N}(\pi^{(t)} - \eta^{(t)} g^{(t)})$ .  
 5: **end while**  
 6: **return**  $\pi^{\text{opt}} = \frac{1}{T} \sum_{t=0}^T \pi^{(t)}$ .

---



---

**Algorithm 3** Adjoint particle tracing for computing  $L_1$  and  $I_1$ .
 

---

1: Let  $\mathbf{x}_0$  be the location where the laser hits  $\partial S$ .  
 2:  $\mathbf{x} \leftarrow \mathbf{x}_0, \omega \leftarrow \omega_L, t \leftarrow 1, C_1 \leftarrow \emptyset$ .  
 3: **while** true **do**  
 4:    $t \leftarrow t \cdot a$ .  
 5:   Sample  $s$  from pdf  $p(s) = \sigma_t \exp(-\sigma_t s)$ .  
 6:    $\mathbf{x}' \leftarrow \mathbf{x} + s \cdot \omega$ .  
 7:   **if**  $\mathbf{x}' \notin S$  **then**  
 8:     **break**  
 9:   **end if**  
 10:   Cache the particle location  $C_1 \leftarrow C_1 \cup \{(\mathbf{x}, \omega)\}$ .  
 11:   Let  $\psi_1$  be the direction connecting  $\mathbf{x}'$  and the camera.  
 12:   Let  $\mathbf{y}_1$  be the intersection of ray  $(\mathbf{x}', \psi_1)$  and the image sensor.  
 13:    $v_1 \leftarrow t \cdot p(\psi_1^T \omega) \cdot \exp(-\sigma_t \|\mathbf{x}' - \mathbf{y}_1\|) \cdot P_0 c/A$ ,  
    where  $c$  is the total number of pixels on the sensor,  $A$  is the sensor’s surface area, and  $P_0$  is the source power.  
 14:   Add  $v_1$  to the corresponding pixel on the image sensor.  
 15:   Sample a direction  $\psi_2$  according to the phase function  $p$ .  
 16:    $\mathbf{x} \leftarrow \mathbf{x}', \omega \leftarrow \psi_2$ .  
 17: **end while**

---



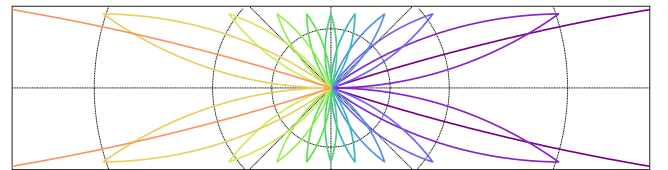
---

**Algorithm 4** Importance sampling for computing  $L_2$ .
 

---

1:  $C_2 \leftarrow \emptyset$   
 2: Uniformly sample a pair  $(\mathbf{x}_0, \omega_0) \in C_1$ .  
 3:  $\mathbf{x} \leftarrow \mathbf{x}_0, \omega \leftarrow \omega_0$ .  
 4:  $\mathbf{x} \leftarrow \mathbf{x} + h\omega$ .  
 5: Sample  $u$  uniformly in  $(0, 1)$ .  
 6: **if**  $u < h(\sigma_{t,k} - \sigma_{s,k})$  **then**  
 7:   **terminate**  
 8: **end if**  
 9: **if**  $h(\sigma_{t,k} - \sigma_{s,k}) < u < h\sigma_{t,k}$  **then**  
 10:   Sample a direction  $\psi$  according to the phase function  $p_k$ .  
 11:    $\omega \leftarrow \psi$ .  
 12: **end if**  
 13: Cache the particle location  $C_2 \leftarrow C_2 \cup \{(\mathbf{x}, \omega)\}$ .

---



**Figure 3:** Phase functions in a tent dictionary with  $N = 10$  atoms (each atom is colored uniquely for better visualization). To be valid probability distributions on the sphere, the atoms are normalized to satisfy Equation 2, and thus have varying magnitudes. The atoms centered at  $0^\circ$  and  $\pi^\circ$  are shown cropped.

function component of the materials and then address the extinction and scattering components.

**Phase functions.** To allow the dictionary to be as general as possible, we aim to be able to express any phase function, that is, any cylindrically symmetric probability distribution on the sphere. Hence, we simply model the phase function as a piecewise linear

function of  $\theta$ . Then, we can use a set of tent (triangular) functions, spaced equally over angular domain  $\theta \in [0, \pi]$ , to approximate it. Denoting the bins number by  $N$  and the bin spacing by  $\theta_s = \pi / (N - 1)$ , we use tent functions of width  $2\theta_s$  and centered at points  $\theta_n = (0, \theta_s, 2\theta_s, \dots, \pi)$ . Each of the tent functions is normalized to satisfy the constraint of Equation (2). In Figure 3, we show the phase functions in a tent dictionary with  $N = 10$ . In our experiments, we use  $N = 200$ , which corresponds to a discretization step of  $0.9^\circ$ .

To avoid high frequency artifacts in the phase function solution we include in Equation (14) a quadratic regularization on its derivatives  $\sum_n (\pi_n - \pi_{n+1})^2$ .

**Extinction and scattering coefficients.** The definition of the atoms' extinction and scattering coefficients should ensure that the dictionary can represent materials with a wide range of  $\sigma_t, \sigma_s$  values. We select an upper bound  $\sigma_{t,\max}$  on the desired extinction coefficients. Note that each scattering function of the form  $\{\sigma_t, \sigma_s, p(\theta)\}$  with  $0 \leq \sigma_t \leq \sigma_{t,\max}$  and  $0 \leq \sigma_s \leq \sigma_t$ , lies on the simplex spanned by  $\{\sigma_{t,\max}, \sigma_{t,\max}, p(\theta)\}$ , the purely absorptive atom  $\{\sigma_{t,\max}, 0, \emptyset\}$ , and an atom of the form  $\{0, 0, \emptyset\}$  describing scattering-free propagation in vacuum. We use the symbol  $\emptyset$  to indicate that the last two atoms are independent of phase function (the phase function is undefined for these two media).

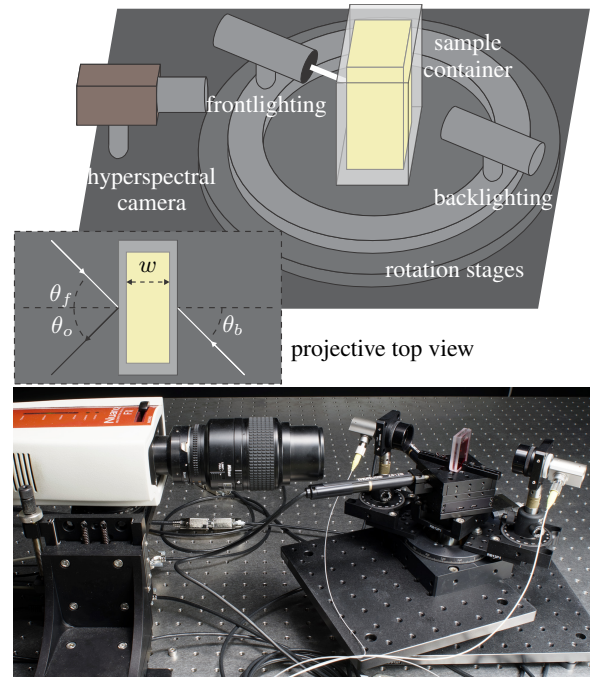
Therefore, we create a scattering dictionary including 200 atoms of the form  $\{\sigma_{t,\max}, \sigma_{t,\max}, p_n(\theta)\}$  with the  $p_n(\theta)$  defined above, plus the two purely absorptive atoms  $\{\sigma_{t,\max}, 0, \emptyset\}$  and  $\{0, 0, \emptyset\}$ . In our experiments we set  $\sigma_{t,\max} = 200 \text{ mm}^{-1}$ , based on the results from Section 6.2.

**Other parameterizations:** Our specific choice of dictionary is aimed to represent any general phase function shape. Depending on the application, other dictionaries may be more appropriate, and some examples include: zonal spherical harmonics for low-frequency phase functions, phase functions derived from Mie theory [Bohren and Huffman 1983; Frisvad et al. 2007] when measuring dispersions, and compact dictionaries such as a set of a few Henyey-Greenstein and von Mises-Fisher functions [Gkioulekas et al. 2013] when a simple phase function model is sufficient. A small adaptation can also allow differentiating directly with respect to the single parameter of a Henyey-Greenstein function (the average cosine). Our optimization framework is quite attractive even for retrieving such simpler phase functions, since it alleviates the need for input measurements which isolate single scattering events.

## 5 Acquisition Setup Design

The optimization strategy described above is general enough to be applied to captured data with any geometry, as long as we can calibrate the 3D shape of the material, the relative position of the camera and light source, and the indices of refraction of the scattering material and its surroundings. Below we describe the physical acquisition setup we built, which is motivated by the simplicity of this calibration process and by some considerations related to the stability of the optimization problem. Inspiration is also drawn from analogous designs in [Jensen et al. 2001; Goesele et al. 2004; Wang et al. 2008] and physics [Johnson and Gabriel 1994]. A schematic and a photograph of our acquisition setup are shown in Figure 4. Further implementation details are provided in Appendix D.

**Geometry.** We cast the material we are interested in measuring into glass cells of variable thickness  $w$ . This allows us to create box-shaped material samples whose exact shape is known with very high accuracy. Furthermore, using micron-accurate smooth glass surfaces means that transition and refraction at the various material interfaces (material and glass, glass and air) can be easily simulated



**Figure 4:** Setup for scattering parameter acquisition. A sample cell is illuminated by collimated beams and imaged by a camera. Rotation stages to achieve arbitrary combinations of lighting and viewing directions. Top: schematic; bottom: implementation.

using Fresnel refraction and reflection laws. In our experiments, we use cells of widths  $w = 1, 2.5, 5, \text{ and } 10 \text{ mm}$ .

**Imaging and lighting.** We use an approximately orthographic camera with a high magnification macro lens ( $4.3^\circ$  subtended angle and  $1 : 3$  reproduction ratio) to sample the light field produced by the material volume. We use narrow (1 mm diameter) collimated beams to illuminate the sample. We use a configuration that allows illuminating either the sample surface imaged by the camera (frontlighting), or its opposite (backlighting). Through a combination of two motorized rotation stages, we can achieve different combinations of front and back lighting directions  $\theta_f, \theta_b$  and viewing directions  $\theta_o$ . In our experiments, we use all possible combinations of  $\theta_f, \theta_b, \theta_o \in \{5^\circ, 15^\circ, 25^\circ\}$ , resulting in a set of 18 measurements per sample, 3 viewing directions times 3 frontlighting plus 3 backlighting directions.

The above combination of sample shape, camera, and illumination lends itself to accurate calibration. In Appendix C we justify the use of collimated beams mathematically. Similar to the BRDF arguments of Ramamoorthi and Hanrahan [2001], we argue that to maximize angular information the configuration should have broadband angular frequency content, and hence be as close as possible to a delta function. The use of both frontlighting and backlighting is motivated by the understanding that a backlighting beam produces measurements dominated by high-order scattering; such measurements are intuitively useful for determining the optical thickness of the material. Conversely, frontlighting results in measurements where low-order scattering is significant, and therefore is informative for the recovery of the material phase function.

**Multi-chromatic measurements.** Scattering parameters vary as functions of wavelength, and this spectral dependency can create perceptually important effects in appearance [Fleming and Bühlhoff 2005; Frisvad et al. 2007]. To capture spectral variations we use monochromatic laser light at three RGB wavelengths, 488, 533, 635 nm, and solve the optimization problem of Equa-

tion (14) independently for each wavelength.

**Index of refraction.** To calibrate for the unknown material’s index of refraction, we use a set of additional measurements with back-lighting such that  $\theta_0 = \theta_b$  (corresponding to direct observation of the source in the absence of a medium). By measuring the shift in the location of the point-spread-function peak caused by refraction in these images, we can easily solve for the material index of refraction at each of the three wavelengths we use. We discuss this process in more detail in Appendix D. We have found our measurement procedure to be adequately accurate for our purposes, but if necessary more accurate measurements of the material index of refraction can be obtained using a refractometer. Additionally, in experiments on synthetic data, we found that small perturbations of the index of refraction ( $\pm 0.1$ ) did not affect recovered scattering parameters considerably.

## 6 Experiments

We now demonstrate and validate our approach for acquiring scattering parameters. We begin with evaluations on synthetic data aimed at understanding the characteristics of our optimization problem. We then show results on two sets of measured materials. The first is a “validation set” of carefully-constructed nano-dispersions whose scattering parameters can be computed using Lorenz-Mie theory; this set provide a means for quantitative validation. The second set consists of everyday materials that are evaluated by their ability to produce accurate rendered images for novel geometries.

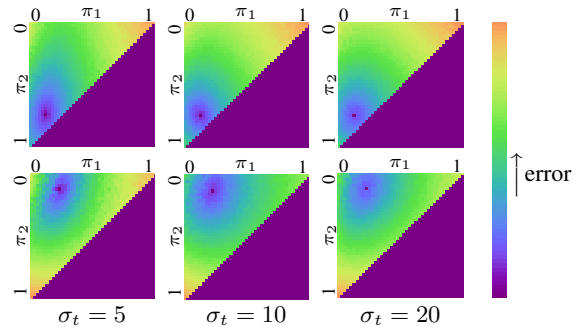
### 6.1 Capture and computation time

We first provide some quantitative information for the acquisition and inversion stages of our measurement pipeline. At the acquisition stage, as described in Section 5, for a single material we take measurements at three wavelengths and a set of 18 different scene configurations, for a total of 54 measurements. Each of these measurements is a high-dynamic range (HDR) image, composited from low-dynamic range images captured at 19 different exposures. In addition, for every material we measure, we capture a set of low-dynamic range calibration images. This process results in a total capture time of approximately 75 minutes per material. We provide more details about the calibration and high-dynamic range imaging procedures in Appendix D.

At the inversion stage, we solve the optimization problem of Section 4 on Amazon EC2 clusters of 100 nodes, with 32 computational cores and at least 20 GB of memory per node (required for the caching of intermediate light fields, as described in Section 4.2). We use the nodes to distribute the outer loop of Algorithm 1, that is, the gradient computation for each dictionary atom (for a dictionary of  $N = 200$  atoms, each node is responsible for two atoms). The results are accumulated at a single master node, which then performs the gradient step of Algorithm 2, and the process is repeated for the number of iterations required until convergence is achieved. We found that processing one set of measurements requires approximately 200 iterations of the SGD algorithm. Overall, fitting one wavelength for a single material requires three to six hours, depending on the density of the material. We use our own C/C++ implementation, which we have optimized through experiments on synthetic data. However, computation could be reduced by further fine-tuning the various parameters involved, such as dictionary, camera spatial resolution, number of iterations, number of samples per rendering, and so on.

### 6.2 Experiments with Synthetic Data

The optimization problem of Section 4 involves the inversion of a random walk process that includes multiple scattering events and is



**Figure 5:** The error surface for 2D optimization problems. We consider a dictionary of three phase functions whose mixing weights lie on the simplex. The simplex is parameterized by its first two coordinates. Columns show results for three reference  $\sigma_t$ , and the rows show two different points as the correct reference in this space.

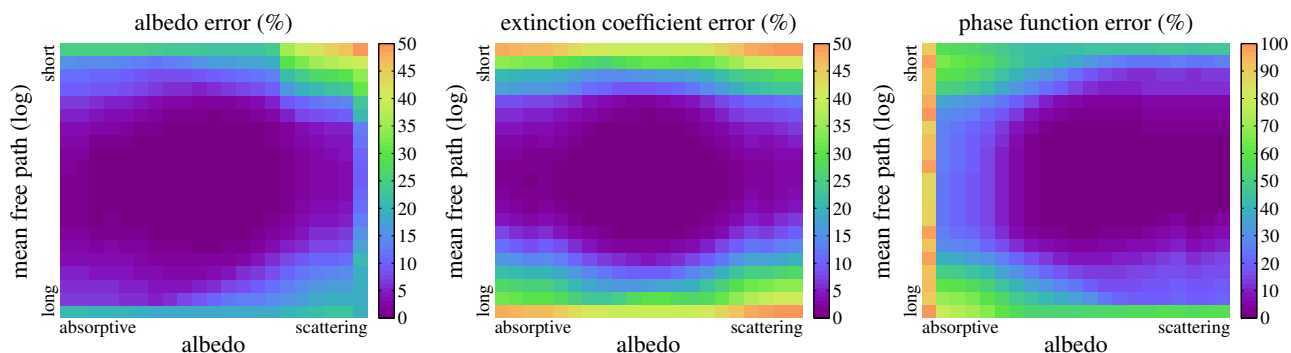
highly non-linear. Despite this, we almost always see in our experiments convergence to a solution that explains the measured data very well. This suggests that the error surface is fairly smooth. To provide more insight, we conduct a series of simulation experiments in which input image-sets are generated using small, artificial three-element dictionaries. Since the three mixing weights are constrained to a simplex, the set of phase functions spanned by three elements is a 2D space, allowing the entire cost surface to be visualized. For these experiments, we parameterize the 2D phase function space by the weights on the first two atoms ( $\pi_1, \pi_2$ ), and in each experiment we choose a “ground truth” phase function ( $\pi_1^*, \pi_2^*$ ) and compute for each  $(\pi_1, \pi_2)$  the  $\mathcal{L}^2$ -difference between input images rendered with that phase function  $\{I^m(\pi_1, \pi_2)\}_{m=1\dots M}$  and those rendered with the true one  $\{I^m(\pi_1^*, \pi_2^*)\}_{m=1\dots M}$ .

Results from six representative experiments are shown in Figure 5. Each row shows three separate experiments in which the true phase function is the same while the optical density  $\sigma_t$  differs. We find that the error surface has a clear minimum at the true value in all of these 2D experiments, and while an exact proof remains a subject for future research, the cost function appears to be very smooth and without spurious local minima, at least for these 2D problems.

In the next experiment with synthetic data, we compare accuracy on absorbing materials versus scattering materials, and on materials with varying optical densities. We consider a large set of artificial materials that are combinations of: (i)  $\sigma_t$  values sampled logarithmically in the interval  $[0.01, \dots, 200 \text{ mm}^{-1}]$ , for a total of 21 values; (ii)  $\sigma_s$  values corresponding, for each  $\sigma_t$ , to 21 albedo values, linearly sampled between  $a = 0$  (purely absorptive) and  $a = 1$  (purely scattering); and (iii) a set of eight different phase functions spanning a wide range of shapes. For each artificial material we render synthetic images using geometry that matches our setup (Section 5) with a sample width of  $w = 1 \text{ mm}$ . Sensor noise is an important consideration for this analysis, so we simulate image noise using photon (Poisson) noise with the parameters reported for two different commercial DSLR cameras [Hasinoff et al. 2010] (which is very large relative to the Monte Carlo rendering error). The noisy images are input to our optimization algorithm, and we measure error between the recovered parameters and the true ones. We use a tent dictionary with  $N = 200$  atoms.

Figure 6 provides a summary of these experiments, by visualizing separately the relative error between the estimated and true values of (left to right): albedo  $a = \sigma_s/\sigma_t$ , extinction coefficient  $\sigma_t$ , and phase function  $p(\theta)$ . Each point in these tables corresponds to the percent error—averaged over the eight true phase function shapes—for distinct values of true albedo (horizontal axis) and extinction coefficient (vertical axis). These tables reveal which types of materials we can expect to measure accurately with our setup. Traveling from





**Figure 6:** Accuracy in the recovery of material parameters. The plots show recovery errors for albedo, extinction coefficient, and mean error for phase function, as a function of different values of albedo  $a = \sigma_s/\sigma_t$  and mean free path  $d = 1/\sigma_t$ .

left to right in these tables makes a gradual transition from purely absorbing materials to purely scattering ones. Traveling from bottom to top moves through materials of increasing optical density, with the top being materials whose mean free path is two hundred times smaller than the sample width  $d = 1/\sigma_t = w/200$ , and the bottom being materials whose mean free path is one hundred times larger than the sample width  $d = 1/\sigma_t = 100w$ .

The first observation—based on the large, low-error regions in the center of the tables—is that estimation is accurate for a wide range of optical densities. This is a useful fact because it means the width of the glass cell need not be chosen with excessive care. We expect very accurate results as long as the sample width is within an order of magnitude of the material’s mean free path, and we expect graceful degradation when the width extends beyond this in either direction. For extremely optically-thin materials (lower rows in table), scattering events become very rare, and images are dominated by noise. For extremely optically-thick materials (top rows), the diffusion approximation [Jensen et al. 2001] becomes applicable, and recovering both the phase function and the scattering coefficient becomes ill-posed. In practice, we simply choose the width for each material sample from a discrete set of available glass cells (1, 2.5, 5, 10 mm) so that they look reasonably translucent under natural light; see examples in Figure 7.

Errors induced by extreme optical thinness and thickness at the top and bottom of these tables should be interpreted differently. If a material is excessively thin at sample width  $w$ , it is relatively easy to instead use a glass cell that is larger. This is less true for materials that are excessively dense, however, since it is physically challenging to cast materials into glass cells that are too small ( $w < 1$  mm). Thus, in cases of extreme optical thickness, our setup will not provide material parameters that can accurately predict appearance on arbitrary geometries, but only for novel geometries at least as wide as the measured sample.

As expected, we also observe large errors in the estimated phase function when materials are extremely absorptive (left column of third table in Figure 6). These errors are somewhat of a computational artifact and have a limited impact on visual appearance. They occur because the appearance of these materials is dominated by attenuation due to absorption, so very little scattering is observed and there is little discernible information about the shape of the phase function. These errors do not impact our ability to predict material appearance, however, because the phase function makes little difference. Indeed, for purely absorptive materials (left-most column) there is no scattering at all, and the phase function can be defined arbitrarily without having any effect on appearance.



**Figure 7:** Measured materials in glass cells of width  $w = 1, 10$ , and 2.5 mm, from left to right. It is not necessary for all of the cell to be filled, as long as there exists a homogeneous region of size comparable to the beam diameter (e.g., hand cream).

### 6.3 Validation materials

It is common in graphics to evaluate measured scattering parameters by demonstrating renderings of visually plausible results. This is an important benchmark, but it does not directly assess the accuracy of the recovered physical parameters. Since our goal is to produce parameters that are faithful to the true mean free path lengths and phase functions in an absolute sense, being able to directly validate the scattering parameters is crucial.

To achieve comparison to “ground truth” parameters, we capture liquid materials whose exact physical structure are known, similar to materials that are used to calibrate instruments used in a variety of domains for particle sizing or estimating molecular weight [Johnson and Gabriel 1994; Pine et al. 1990]. They are created by dispersing nano-scale spherical particles of known chemical composition into a homogeneous embedding medium of a different refractive index, using procedures that allow for very precise control of particle concentration, particle size distribution, and homogeneity. Given these parameters, Lorenz-Mie theory [Bohren and Huffman 1983; Frisvad et al. 2007] provides analytic expressions of the bulk material scattering parameters  $\{\sigma_t, \sigma_s, p(\theta)\}$  at any wavelength.

We measure nanodispersions of two types. First, we measure dispersions of polystyrene spheres in water that are almost monodisperse (single particle size) and are precise enough to be traceable to NIST Standard Reference Materials. We measure three such dispersions<sup>2</sup>, each having a 1% ( $w/v$ ) concentration of particles at a different particle radius: 200, 500, or 800 nm. Second, we measure a spherical polydispersion of aluminum oxide particles ( $Al_2O_3$ ) in water<sup>3</sup>, with an approximately known particle size distribution in

<sup>2</sup>Nanobead NIST Traceable Particle Size Standards, Polysciences, Inc.

<sup>3</sup>NanoArc Aluminum Oxide, Nanophase Technologies Corporation.

the range 20 – 300 nm and mean radius of 30 nm. We use glass cells of width  $w = 1$  mm for all of these measurements, and instead of estimating the indices of refraction from image data, we use those predicted by Lorenz-Mie theory.

The results of our measurements are shown in Table 1. In all cases, the error in the recovered parameters is less than 5%. (Note that these materials are purely scattering, so  $\sigma_t = \sigma_s$ .) The largest error occurs for the aluminum oxide material, for which the particle size distribution is known much less precisely. Figure 8-left compares the green-channel phase functions recovered by our optimization (purple curves) to the ground truth phase functions predicted by Lorenz-Mie theory (dotted orange curves). We see that the matches are extremely close. As a reference, we compare both to Henyey-Greenstein phase functions; as the single parameter  $g$  of an HG phase function is equal to its average cosine, we plot (green curves) the HG phase function that have  $g$  values that are equal to the average cosine of the ground truth phase function. We note that their shapes deviate significantly from the ground-truth. This deviation is important for appearance, particularly for objects that have thin geometry with low-order scattering, where the phase function plays an important role visually. The middle columns demonstrate this by showing captured and fit (pseudo-colored) images of the materials under frontal laser illumination at a new angle (which was not used in optimization). The rightmost column shows cross-sections of the image intensities. The deviations of the HG fits from ground-truth lead to discernible differences between the images.

These experiments highlight the fact that simple, single-parameter phase function models can be insufficient for modeling the appearance of scattering materials, and it justifies our choice to fit higher-dimensional phase function models.

#### 6.4 Other materials

Next, we use our acquisition setup and optimization algorithm to measure several common materials. They can be grouped roughly into three categories:

- Highly scattering liquids of varying viscosities; including mustard, shampoo, hand cream, liquid designer clay, and different types of milk.
- Highly absorbing liquids with limited scattering; including coffee, robittussin, olive oil, blue curacao liquor, and red wine.
- Solids that can be molded into the glass cells; such as different types of soap.

By “eyeballing” each sample under natural light, we choose glass cell widths so that each sample looks reasonably translucent under ambient lighting. The results we report were captured using width  $w = 1$  mm for materials in the first and third categories, except for glycerine soap; and  $w = 10$  mm for the second category and glycerine soap. Photographs of samples in 1 mm, 2.5 mm, and 10 mm cells are shown in Figure 7. For each sample, we estimate the index of refraction as described in Section 5, and these range from values of 1.33 (for milk, reduced milk, milk soap, and the water soluble liquids) to 1.47 (for olive oil and glycerine).

The measured parameters are shown in Table 2. We quantitatively evaluate the quality of the recovered scattering parameters in two ways. First, we report the *fitting error*, which is the average  $\mathcal{L}_2$  image difference between input images and the corresponding images rendered with the recovered parameters, normalized by the  $\mathcal{L}_2$ -norms of the input images. Second, we compute a measure of *generalization error* by: i) using the recovered parameters to render laser-illumination images with different sample widths and lighting directions; and ii) comparing these simulated images to captured

photographs in these same novel configurations. For the novel configurations, we use lighting angles  $\theta_f, \theta_b \in \{10^\circ, 20^\circ, 30^\circ\}$  and glass cells with widths  $w \in \{2.5, 5 \text{ mm}\}$ . The generalization error for each material is reported as the average relative  $\mathcal{L}_2$  image difference over the set of all novel configurations. As shown in the right two columns of Table 2, fitting errors are less than 4% and generalization errors below 5%.

Figure 9 shows the measured phase functions, each superimposed with an HG phase functions whose  $g$ -value is equal to the average cosine of the phase function we measure. Some of these phase functions are well approximated by the HG model but others, including hand cream, liquid clay, and mixed soap, are not. This set of tabulated phase functions is available at the project website.

As qualitative evaluation, Figure 1-right shows an image rendered with our recovered material parameters under natural lighting. From left to right, are milk soap and glycerine soap (top and bottom, respectively), olive oil, blue curacao, and reduced milk. The soap geometry corresponds to scanned molded cubes made of the corresponding materials. We see that the recovered material parameters successfully reproduce the color variations that are critical to the translucent appearance of these materials. This is most notable in the glycerine soap, where blue wavelengths scatter first and cause a reddish glow in the middle of the object, but it is also visible on the left edge of the milk soap and the top-right corner of the milk. A high-resolution version of Figure 1 and a visualization that highlights the color variations are shown in Appendix E. The scene file used for this figure is available at the project website.

## 7 Conclusions

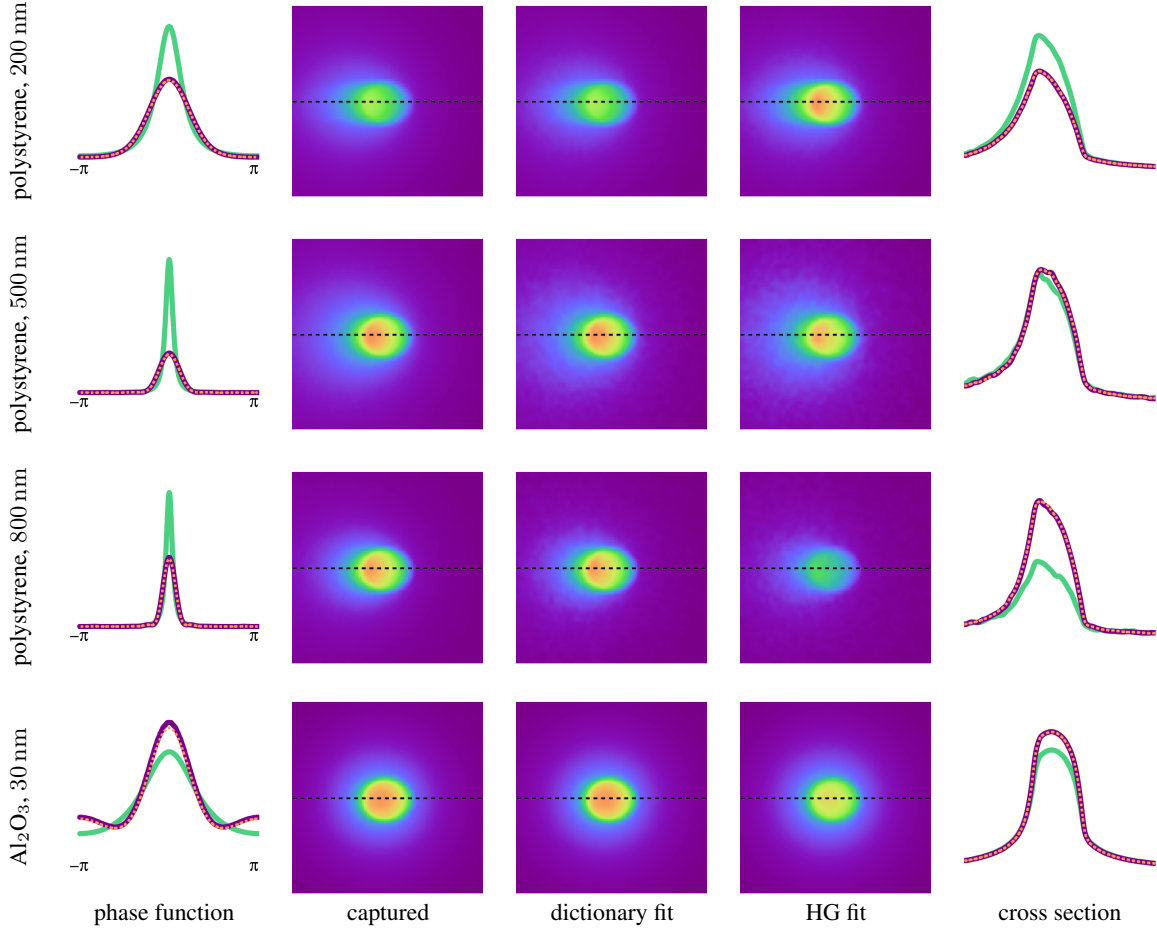
We present an optimization framework for inverting the effect of multiple-scattering to recover scattering properties of homogeneous volumes from a handful of images. The approach does not require precise isolation of single scattering, and this enables the measurement of a broader set of materials, including both solids and liquids. The optimization also incorporates a large material dictionary and thereby avoids the restrictions of low-parameter phase function models. Our analysis and experiments show that we can recover accurate physical scattering parameters for a variety of materials.

Our current setup and optimization framework do not account for polarization or fluorescence phenomena. Polarization can be important for the appearance of materials with strongly polarization-dependent scattering properties or index of refraction (birefringence), such as crystalline materials. Experimentally, our optimization has been unable to find scattering parameters that match our setup’s images of microcrystalline wax, and this may be due to some combination of our simulator’s ignorance of polarization and our use of partially-polarized (laser plus fiber) light. Regarding fluorescence, we have verified that it has negligible impact on our measurements of the materials listed in Section 6. Our setup can be easily modified to measure the strongly fluorescent behavior of other materials, by including in addition to the hyperspectral camera a mechanism to control wavelength at the source side.

While we proposed one possible scanning configuration, our optimization could be used to infer scattering parameters from images captured from a variety of scene geometries and incident light fields. The only requirement is that both lighting and geometry be precisely calibrated. Our setup combines the benefits of high-frequency angular lighting (for stable optimization) and precise, stable calibration (for repeatability), but it limits measurements to three wavelengths and to solids that can be cast into glass cells of thickness within an order of magnitude of the mean free path. In principle, our optimization could be applied to images of more general solid objects, but this would require enhancing our setup to also

dispersion	$\sigma_s$ predicted			$\sigma_s$ measured			$\sigma_s$ error (%)			phase function error (%)		
	R	G	B	R	G	B	R	G	B	R	G	B
polystyrene, 200 nm	17.220	28.363	36.517	17.078	28.650	36.823	0.825	1.012	0.838	3.031	1.143	3.672
polystyrene, 500 nm	59.082	79.557	88.626	58.431	79.023	88.062	1.102	0.671	0.636	3.181	2.676	1.359
polystyrene, 800 nm	65.757	70.438	68.589	66.976	71.544	69.146	1.853	1.570	0.812	2.623	2.117	1.251
Al <sub>2</sub> O <sub>3</sub> , 30 nm	47.341	93.389	129.870	48.536	96.004	132.695	2.524	2.800	2.175	3.712	4.298	3.108

**Table 1:** Measurements of validation materials (controlled nano-dispersions). Values for  $\sigma_s$  are reported in ( $\text{mm}^{-1}$ ). Phase function error is given as  $\mathcal{L}_2$  difference normalized by the  $\mathcal{L}_2$ -norm of the reference phase function. All four validation materials have negligible absorption, resulting on both the predicted and measured values for  $\sigma_t$  to agree with those we report for  $\sigma_s$  to the third decimal.



**Figure 8:** Measurements of validation materials (controlled nano-dispersions). Left: For each material, we show for the green wavelength the theoretically predicted (dashed orange) and recovered (purple) phase functions, as well as the best Henyey-Greenstein (green) phase function fit. The recovered phase functions are in close agreement with the correct ones and the purple and orange curves tightly overlap. As another visualization, we show the images for a novel configuration: under frontal collimated laser illumination ( $\theta_f = 25^\circ, \theta_o = 0^\circ$ ). We compare our phase function and the best Henyey-Greenstein fit (images are color-mapped for better visualization). The rightmost column shows a crosssection through the captured and re-rendered images for this configuration.

recover the object shape and its surface microstructure (BSDF).

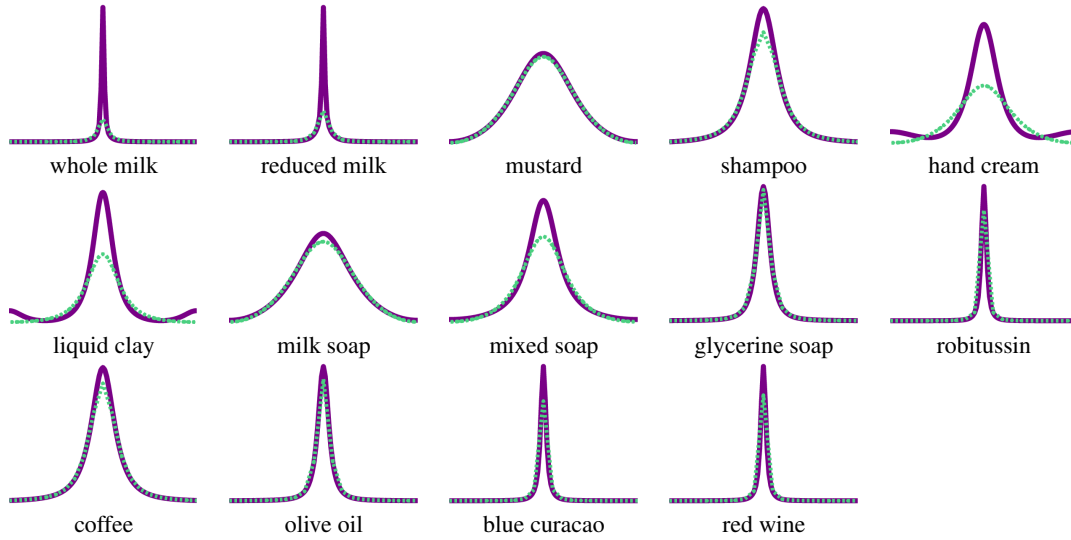
In addition, combinations of our optimization framework with more sophisticated imaging configurations could improve the optimization’s stability and convergence rate. In particular, it may be fruitful to apply our optimization to images captured with high-frequency illumination [Mukaigawa et al. 2010], basis illumination [Ghosh et al. 2007], adaptive illumination [O’Toole and Kutulakos 2010], or transient imaging [Wu et al. 2012]. It is also possible that optimization schemes like ours will allow exploiting such imaging modalities to solve more challenging inverse problems, such as measuring heterogeneous scattering media.

## Acknowledgments

We thank Henry Sarkas at Nanophase for donating material samples and calibration data. Funding by the National Science Foundation (IIS 1161564, 1012454, 1212928, and 1011919), the European Research Council, the Binational Science Foundation, Intel ICRI-CI, and Amazon Web Services in Education grant awards. Much work was performed while T. Zickler was a Feinberg Foundation Visiting Faculty Program Fellow at the Weizmann Institute.

material	$\sigma_s$			$\sigma_a$			first moment			fitting error (%)	generalization error (%)
	R	G	B	R	G	B	R	G	B		
whole milk	100.920	105.345	102.768	0.013	0.013	0.041	0.954	0.963	0.946	2.0460	3.6344
reduced milk	57.291	62.460	63.757	0.007	0.007	0.024	0.954	0.957	0.942	1.346	2.039
mustard	16.447	18.536	6.457	0.057	0.061	0.451	0.155	0.173	0.351	3.377	4.201
shampoo	8.111	9.919	10.575	0.178	0.328	0.439	0.907	0.882	0.874	3.962	4.752
hand cream	20.820	32.353	41.798	0.011	0.011	0.012	0.188	0.247	0.265	2.652	3.221
liquid clay	37.544	48.250	67.949	0.004	0.004	0.005	0.312	0.442	0.512	3.431	4.532
milk soap	7.625	8.004	8.557	0.003	0.004	0.015	0.164	0.167	0.155	1.895	2.956
mixed soap	3.923	4.018	4.351	0.003	0.005	0.013	0.330	0.322	0.316	1.474	3.316
glycerine soap	0.201	0.202	0.221	0.001	0.001	0.002	0.955	0.949	0.943	3.840	3.920
robitussin	0.009	0.001	0.001	0.012	0.197	0.234	0.906	0.977	0.980	1.379	3.998
coffee	0.054	0.051	0.049	0.275	0.309	0.406	0.911	0.899	0.906	1.957	2.199
olive oil	0.041	0.039	0.012	0.062	0.047	0.353	0.946	0.954	0.975	2.287	3.846
blue curacao	0.010	0.012	0.021	0.083	0.048	0.011	0.955	0.973	0.979	2.704	4.857
red wine	0.015	0.013	0.011	0.122	0.351	0.402	0.947	0.975	0.977	3.034	3.192

**Table 2:** Scattering parameters of materials measured using our proposed acquisition setup and inversion algorithm. Values for  $\sigma_s$  and  $\sigma_a$  are reported in  $(\text{mm}^{-1})$ . The average cosine of the measured phase functions is reported, while the entire phase functions are shown in Figure 9. Fitting and generalization errors are given as %  $\mathcal{L}_2$  difference normalized by the  $\mathcal{L}_2$ -norm of the reference image, averaged across the fitting and novel captured images respectively.



**Figure 9:** Phase functions of materials measured using our acquisition setup (purple), contrasted with the closest HG phase function (dashed green). See Table 2 for numerical values.

## A Volume Rendering Equation

Volume rendering is commonly formulated in terms of the *volume rendering equation* [Jensen 2001]. Before showing the volume rendering equation, we first introduce some notation.

We assume that light fields  $L$  are functions on the space  $S \times \mathbb{S}^2$ , where  $S$  a convex subset of the Euclidean space  $\mathbb{R}^3$  occupied by a scattering material volume, and  $\mathbb{S}^2$  is the two-dimensional unit sphere (sphere of directions). We also assume that the incident radiance  $L(\mathbf{x}, \boldsymbol{\omega})$  is known for all  $\mathbf{x}$  on the boundary  $\partial S$  of  $S$  and directions  $\boldsymbol{\omega} \in \mathbb{S}^2$  entering the medium  $S$ . We denote points on a half-line (ray) starting at a point  $\mathbf{x} \in S$  and with direction vector  $\boldsymbol{\omega} \in \mathbb{S}^2$  as  $\mathbf{y}_r(\mathbf{x}, \boldsymbol{\omega}) = \mathbf{x} - r\boldsymbol{\omega}$ , for  $r > 0$ . Because  $S$  is convex, we know that for every such half-line there exists a unique  $r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})$  such that the line intersects the boundary  $\partial S$ , at a point which we denote  $\mathbf{y}_{\partial S}(\mathbf{x}, \boldsymbol{\omega})$ .

Similar to Equation (4), the volume rendering equation is also derived from the RTE (Equation (1)). Instead of using the finite-difference approximation of Section 3.1, it is obtained by integrating both sides of the RTE [Ishimaru 1978]; using the notation we

introduced, for a homogeneous material  $k = \{\sigma_t, \sigma_s, p(\theta)\}$ , it can be written in the form

$$\begin{aligned}
 L(\mathbf{x}, \boldsymbol{\omega}) = & \exp(-\sigma_t r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})) L(\mathbf{x} - r_{\partial S}(\mathbf{x}, \boldsymbol{\omega}), \boldsymbol{\omega}) \\
 & + \int_0^{r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})} \exp(-\sigma_t r') \left( Q(\mathbf{x} - r'\boldsymbol{\omega}, \boldsymbol{\omega}) \right. \\
 & \left. + \sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\psi}^T \boldsymbol{\omega}) L(\mathbf{x} - r'\boldsymbol{\omega}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}) \right) dr'.
 \end{aligned} \tag{22}$$

where  $Q(\mathbf{x} - r'\boldsymbol{\omega}, \boldsymbol{\omega})$  is a volume emission term, to be discussed later. We define the *input term*

$$\begin{aligned}
 L_{V,i}(\mathbf{x}, \boldsymbol{\omega}) \triangleq & \exp(-\sigma_t r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})) L(\mathbf{x} - r_{\partial S}(\mathbf{x}, \boldsymbol{\omega}), \boldsymbol{\omega}) \\
 & + \int_0^{r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})} \exp(-\sigma_t r') Q(\mathbf{x} - r'\boldsymbol{\omega}, \boldsymbol{\omega}) dr',
 \end{aligned} \tag{23}$$

the *single-scattering operator* (sometimes called *single-bounce op-*

erator)

$$\mathcal{B}_k(L)(\mathbf{x}, \boldsymbol{\omega}) \triangleq \sigma_s \int_0^{r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})} \exp(-\sigma_t r') \int_{\mathbb{S}^2} p(\boldsymbol{\psi}^T \boldsymbol{\omega}) L(\mathbf{x} - r' \boldsymbol{\omega}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}) dr'. \quad (24)$$

and the corresponding volume rendering operator

$$\mathcal{V}_k \triangleq (\mathcal{I} - \mathcal{B}_k)^{-1} = \sum_{j=0}^{\infty} \mathcal{B}_k^j, \quad (25)$$

where in Equation (25) we again used the Neumann series expansion for the second equality. Then, we can use these operators to rewrite the volume rendering equation (22) in operator form as

$$\begin{aligned} L &= L_{V,i} + \mathcal{B}_k L \Rightarrow \\ L &= (\mathcal{I} - \mathcal{B}_k)^{-1} L_{V,i} \Rightarrow \\ L &= \mathcal{V}_k L_{V,i} \end{aligned} \quad (26)$$

At this point, it is worth drawing some analogies between the operator-theoretic formulation of volume light transport presented here, and the one we derived in Section 3.1. The volume rendering operator  $\mathcal{V}_k$  is the counterpart of the rendering operator  $\mathcal{R}_k$  of Equation (8); Equations (26) and Equation (6), respectively, show how each of the two rendering operators can be applied to an appropriate input term to produce the light field inside the volume. Equations (25) and (8) show that both  $\mathcal{V}_k$  and  $\mathcal{R}_k$  have Neumann series expansions, meaning that they be written as the sum of all orders of consecutive applications of a corresponding “single-action” operator. For the volume rendering operator  $\mathcal{V}_k$ , this expansion is in terms of the single-scattering operator  $\mathcal{B}_k$ ; for the rendering operator  $\mathcal{R}_k$ , the expansion is in terms of the single-step propagation operator  $\mathcal{K}_k$ . As we discuss in the following subsection, at the limit  $h \rightarrow 0$  for the step size used in the finite difference approximation of Section 3.1, the volume rendering operator  $\mathcal{V}_k$  and the rendering operator  $\mathcal{R}_k$  are equivalent, in the sense that the light fields at the left hand side parts of Equations (26) and (6) are equal. However, even at that limit, the operators  $\mathcal{K}_k$  and  $\mathcal{B}_k$  used in the Neumann expansion of the two rendering operators are different, and corresponding terms in the two expansions are also different.

### A.1 Relationship with finite-difference approximation

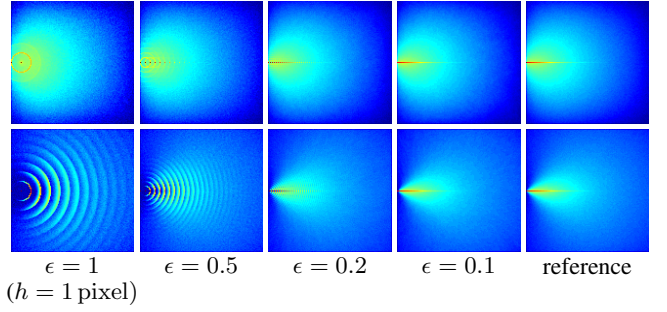
The rendering equation (4), and therefore also its operator form in Equation (6), presented in Section 3.1 can be derived directly from the volume rendering equation (26). In this section, we first show this derivation, and then discuss insights it provides into the finite-difference approximation used for the formulation of Section 3.1.

We can approximate the integrals in Equation (22) using the rectangle method [LeVeque 2007]: assuming a step size  $h = r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})/N$ , we have

$$\begin{aligned} L(\mathbf{x}, \boldsymbol{\omega}) &\approx \exp(-\sigma_t N h) L(\mathbf{x} - N h \boldsymbol{\omega}, \boldsymbol{\omega}) \\ &+ h \sum_{n=1}^N \exp(-\sigma_t n h) \left( Q(\mathbf{x} - n h \boldsymbol{\omega}, \boldsymbol{\omega}) \right. \\ &\left. + \sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\psi}^T \boldsymbol{\omega}) L(\mathbf{x} - n h \boldsymbol{\omega}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}) \right). \end{aligned} \quad (27)$$

Equation (27) can be rewritten equivalently in recursive form as

$$\begin{aligned} L(\mathbf{x}, \boldsymbol{\omega}) &\approx \exp(-\sigma_t h) L(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\omega}) \\ &+ h \exp(-\sigma_t h) \left( Q(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\omega}) \right. \\ &\left. + \sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\psi}^T \boldsymbol{\omega}) L(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}) \right). \end{aligned} \quad (28)$$



**Figure 10:** 2D fluence fields computed using the finite-difference approximation and the standard volume rendering equation: (top) isotropic phase function  $p(\theta) \equiv \frac{1}{4\pi}$ ; (bottom) von Mises-Fisher phase function with  $\kappa = 5$ .

Using the first order approximations  $\exp(-\epsilon) \approx 1 - \epsilon$  and  $\epsilon \exp(-\epsilon) \approx \epsilon$ , and after some algebraic manipulation, Equation (28) becomes

$$\begin{aligned} L(\mathbf{x}, \boldsymbol{\omega}) &\approx h Q(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\omega}) + (1 - h \sigma_t) L(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\omega}) \\ &+ h \sigma_s \int_{\mathbb{S}^2} p(\boldsymbol{\psi}^T \boldsymbol{\omega}) L(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\psi}) d\mu(\boldsymbol{\psi}), \end{aligned} \quad (29)$$

which is identical to Equation (4) for  $L_i(\mathbf{x}, \boldsymbol{\omega}) = h Q(\mathbf{x} - h \boldsymbol{\omega}, \boldsymbol{\omega})$ .

**Input term and boundary conditions.** In the recursion used to arrive at Equation (28) from Equation (27), we need to provide a valid initial condition. The straightforward way to achieve this is to initialize the recursion at the boundary  $\mathbf{x} \in \partial S$ , where the light field  $L(\mathbf{x}, \boldsymbol{\omega})$  for directions  $\boldsymbol{\omega} \in \mathbb{S}^2$  entering the medium  $S$  is fully specified by the scene light sources, and therefore assumed to be known. In this case, the input term  $L_i(\mathbf{x}, \boldsymbol{\omega})$  in Equation (4) (or equivalently Equation (29)) accounts exclusively for the material’s self emission  $Q(\mathbf{x}, \boldsymbol{\omega})$  and does not include external sources.

Alternatively, we can incorporate both the volume emission  $Q(\mathbf{x}, \boldsymbol{\omega})$  and the incident radiance on  $\partial S$  into the input term  $L_i(\mathbf{x}, \boldsymbol{\omega})$ , by defining it as

$$L_i(\mathbf{x}, \boldsymbol{\omega}) = \begin{cases} h Q(\mathbf{x}, \boldsymbol{\omega}) + L_{\partial S}(\mathbf{x}, \boldsymbol{\omega}) \delta(0) & \mathbf{x} \in \partial S, \\ h Q(\mathbf{x}, \boldsymbol{\omega}) & \mathbf{x} \notin \partial S \end{cases} \quad (30)$$

where  $L_{\partial S}(\mathbf{x}, \boldsymbol{\omega})$  is the incident radiance resulting from scene light sources that is, as previously, assumed known. Then, for the purposes of calculating the recursion of Equation (28), we can simply use  $L(\mathbf{x}, \boldsymbol{\omega}) = 0$  for every point  $\mathbf{x}$  outside the material volume. This is the approach we adopted in Section 3.1. It is worth pointing out that the emission term  $Q(\mathbf{x}, \boldsymbol{\omega})$  has units of radiance per unit length, whereas the input term  $L_i(\mathbf{x}, \boldsymbol{\omega})$  has units of radiance; this explains the presence of the multiplier  $h$  (that has units of length) for the emission term in all of the definitions of  $L_i(\mathbf{x}, \boldsymbol{\omega})$  we discussed, including that of Equation (30).

**Step size selection and validity of approximation.** To arrive at Equation (29), we used the first order approximation  $\exp(-h \sigma_t) \approx 1 - h \sigma_t$ . This gives us a practical rule for selecting the step size  $h$  in the finite-difference approximation; namely, for the approximation to be valid, we need to set  $h = \epsilon / \sigma_t$  for some  $0 < \epsilon \ll 1$ . The effect of the choice of  $h$  is shown in Figure 10, where we observe that, for small enough  $h$ , the volume rendering and finite-difference formulations produce equivalent renderings.

## A.2 Dictionary representation for volume rendering equation

As in Section 4.1, we now consider a dictionary of materials  $D = \{k_n, n = 1, \dots, N\}$ , where  $k_n = \{\sigma_{t,n}, \sigma_{s,n}, p_n(\theta)\}$ , and their corresponding single-scattering operators  $\{\mathcal{B}_{k_n}\}$ . Then, the analogous of Lemma 1 does not hold for the convex combinations of the materials in  $D$  and the operators  $\{\mathcal{B}_{k_n}\}$ . That is, for any weight vector  $\pi \in \Delta^N$ , the operator  $\sum_{n=1}^N \pi_n \mathcal{B}_{k_n}$  is not always a valid single-scattering operator for some material; and inversely the single-scattering operator for a material defined by the mixing Equations (12)-(13) is not equal to  $\sum_{n=1}^N \pi_n \mathcal{B}_{k_n}$ . This happens because of the non-linear (exponential) dependence of the spatial component of  $\mathcal{B}_k$  on  $\sigma_t$ .

An analogous of Lemma 1 can be derived, in exactly the same way as that lemma, if we make the additional assumption that all the materials  $k_n$  in the dictionary  $D$  have the same extinction coefficient,

$$\sigma_{t,n} = \sigma_t, n = 1, \dots, N. \quad (31)$$

The consequence of this assumption is that we can no longer infer all material parameters by solving only for a vector of mixing weights  $\pi$ , but also need to optimize over  $\sigma_t$ . Therefore, to do inverse volume rendering through appearance matching, we now need to solve the optimization problem

$$\min_{\pi \in \Delta^N, \sigma_t > 0} \sum_{m=1}^M w_m (S^m (\mathcal{I} - \mathcal{B}(\sigma_t, \pi))^{-1} L_i^m(\sigma_t) - \bar{I}^m)^2, \quad (32)$$

where  $\mathcal{B}(\sigma_t, \pi) = \sum_{n=1}^N \pi_n \mathcal{B}(\sigma_t)_{k_n}$ , and the dependence on  $\sigma_t$  is now explicit and not implicit through the weight  $\pi$ . This is a harder optimization problem than that of Equation (14), which is further complicated by the fact that the parameters  $\sigma_t$  and  $\sigma_s$  appear in  $\mathcal{B}_k$  multiplicatively coupled, meaning that solving the problem of Equation (32) would require alternatingly optimizing over  $\sigma_t$  and  $\pi$ . In addition to worse susceptibility to local minima, these alternating optimization procedures typically require a considerably larger number of gradient descent iterations to converge. These complications are the reason why in Section 4 we select to use the finite difference-based formulation of volume light transport presented in Section 3.1.

## B Simulating Light Transport

In this section we describe a particle tracing algorithm for performing the rendering operations necessary for the optimization problem in Section 4.2. As explained there, each gradient computation requires the following rendering and sampling operations:

1. Render a light field  $L_1$  using the rendering operator  $\mathcal{R}_k$  with input light field  $L_i(\mathbf{x}, \omega)$ .
2. Apply the single-step propagation operator  $\mathcal{K}_k$  to  $L_1$ , producing a light field  $L_2$ .
3. Render a light field  $L_3$ , by applying the full rendering operator  $\mathcal{R}_k$  to  $L_2$ .
4. Apply the sampling operator  $\mathcal{S}$  to  $L_1$  and  $L_3$  to obtain images  $I_1$  and  $I_2$ .

We reproduce later in the section Algorithms 3 and 4 of Section 4.2, for more convenient reference as we derive them in detail.

In our implementation, for the first and third operations we use the volume rendering operator  $\mathcal{V}_k$  instead of the rendering operator  $\mathcal{R}_k$ . As explained in Appendix A, for step size  $h \ll \varepsilon/\sigma_t$  the two operators produce the same output. At the same time, rendering with the

---

**Algorithm 5** Compute  $L^{(I)}(\mathbf{x}, \omega)$ .

---

- 1: Compute  $\mathbf{y} = \mathbf{y}_{\partial S}(\mathbf{x}, \omega)$  using ray tracing.
- 2: Sample a point  $\mathbf{x}'$  on the line segment  $(\mathbf{x}, \mathbf{y})$  from  $p_0(\mathbf{x}')$ .
- 3: Sample a direction  $\psi_1$  from  $p_1$  and compute

$$v_1 = p(\psi_1^T \omega) L^{(D)}(\mathbf{x}', \psi_1) / p_1(\psi_1).$$

- 4: Sample a direction  $\psi_2$  and compute recursively

$$v_2 = p(\psi_2^T \omega) L^{(I)}(\mathbf{x}', \psi_2) / p_2(\psi_2).$$

- 5: **return**  $\exp(-\sigma_t \|\mathbf{x}' - \mathbf{x}\|) \sigma_s (v_1 + v_2) / p_0(\mathbf{x}')$ .
- 

volume rendering operator  $\mathcal{V}_k$  is much faster than rendering with the operator  $\mathcal{R}_k$ , as the many small steps of the latter are replaced with steps of variable size depending on  $\sigma_t$  in the former. Experimentally, we have verified that we get almost identical parameters regardless of which of the two operators we use, but rendering with  $\mathcal{V}_k$  speeds-up computation by almost an order of magnitude for optically thick materials. It is important to note that this replacement is used only for the first and third stage; for the intermediate rendering stage, we use exactly the single-step propagation operator  $\mathcal{K}_k$ .

We next describe how to render the light field  $L_1(\mathbf{x}, \omega)$  from the input light field  $L_i(\mathbf{x}, \omega)$ , and obtain a corresponding image  $I_1$ , using the volume rendering equation. We do this using Monte Carlo integration with *next event estimation* [Lafortune 1996] to improve the performance: first, we split  $L(\mathbf{x}, \omega)$  into a *direct term*

$$L^{(D)}(\mathbf{x}, \omega) = \exp(-\sigma_t r_{\partial S}(\mathbf{x}, \omega)) L(\mathbf{y}_{\partial S}(\mathbf{x}, \omega), \omega) + \int_0^{r_{\partial S}(\mathbf{x}, \omega)} \exp(-\sigma_t r') Q(\mathbf{y}_{r'}(\mathbf{x}, \omega), \omega) dr' \quad (33)$$

and an *indirect term*

$$L^{(I)}(\mathbf{x}, \omega) = L(\mathbf{x}, \omega) - L^{(D)}(\mathbf{x}, \omega); \quad (34)$$

then, we estimate them separately since the direct term  $L^{(D)}(\mathbf{x}, \omega)$  does not depend on the unknown light field  $L(\mathbf{x}, \omega)$ , but only on the (assumed known) radiance sources in the scene, and is easy to compute. Unbiased estimates of the indirect term  $L^{(I)}(\mathbf{x}, \omega)$  can be obtained using the recursive Algorithm 5.

To implement Algorithm 5 efficiently we need to choose the distributions  $p_0(\mathbf{x}')$ ,  $p_1(\psi_1)$ ,  $p_2(\psi_2)$  smartly. Since in our setup the light source that is just one collimated beam, it is more efficient to simulate the ‘dual’ problem, in which the image sensor emits *importance*, which is collected by the light sources in the scene. This is equivalent due to the symmetry of light transport, as justified in detail by Veach [1997].

In step 2 of Algorithm 5, we need to sample a point  $\mathbf{x}'$  along the ray  $(\mathbf{x}, \omega)$ . Namely, we need to sample a distance  $s \geq 0$  and set  $\mathbf{x}' = \mathbf{x} - s \cdot \omega$ . Given the exponential falloff in step 5,  $s$  can be sampled from an exponential distribution with mean  $1/\sigma_t$ :

$$p_0(\mathbf{x}') = p(s) = \sigma_t \exp(-\sigma_t s). \quad (35)$$

In step 4 of Algorithm 5, we can sample  $\psi_2$  directly using the phase function  $p$ . Thus  $p_2(\psi_2) = p(\psi_2^T \omega)$  and  $v_2$  simplifies to  $L^{(I)}(\mathbf{x}', \psi_2)$ .

---

**Algorithm 6** Adjoint particle tracing for computing  $L_1$  and  $I_1$ .

```

1: Let  $\mathbf{x}_0$  be the location where the laser hits  $\partial S$ .
2:  $\mathbf{x} \leftarrow \mathbf{x}_0, \boldsymbol{\omega} \leftarrow \boldsymbol{\omega}_L, t \leftarrow 1, C_1 \leftarrow \emptyset$ .
3: while true do
4:    $t \leftarrow t \cdot a$ .
5:   Sample  $s$  from pdf  $p(s) = \sigma_t \exp(-\sigma_t s)$ .
6:    $\mathbf{x}' \leftarrow \mathbf{x} + s \cdot \boldsymbol{\omega}$ .
7:   if  $\mathbf{x}' \notin S$  then
8:     break
9:   end if
10:  Cache the particle location  $C_1 \leftarrow C_1 \cup \{(\mathbf{x}, \boldsymbol{\omega})\}$ .
11:  Let  $\boldsymbol{\psi}_1$  be the direction connecting  $\mathbf{x}'$  and the camera.
12:  Let  $\mathbf{y}_1$  be the intersection of ray  $(\mathbf{x}', \boldsymbol{\psi}_1)$  and the image sensor.
13:   $v_1 \leftarrow t \cdot p(\boldsymbol{\psi}_1^T \boldsymbol{\omega}) \cdot \exp(-\sigma_t \|\mathbf{x}' - \mathbf{y}_1\|) \cdot P_0 c/A$ ,
    where  $c$  is the total number of pixels on the sensor,  $A$  is the
    sensor's surface area, and  $P_0$  is the source power.
14:  Add  $v_1$  to the corresponding pixel on the image sensor.
15:  Sample a direction  $\boldsymbol{\psi}_2$  according to the phase function  $p$ .
16:   $\mathbf{x} \leftarrow \mathbf{x}', \boldsymbol{\omega} \leftarrow \boldsymbol{\psi}_2$ .
17: end while

```

---

Now we can use Algorithm 6, a specialized version of Algorithm 5, to solve our problem. To sample  $s$  for step 5 of Algorithm 6, we can draw  $\xi$  uniformly from  $(0, 1)$  and set  $s = -\ln \xi / \sigma_t$ . Note that in Algorithm 6, we assume that the camera is orthographic. Thus given a point  $\mathbf{x}'$ , the direction that connects it to the camera is unique. So  $v_1$  can be computed directly without performing any sampling.

To complete the description of the algorithm we need to define the distribution  $p_1(\boldsymbol{\psi}_1)$ . Since  $L^{(D)}(\mathbf{x}, \boldsymbol{\omega})$  will be zero unless the ray is pointing in the sensor direction, we always choose  $\boldsymbol{\psi}_1$  as the direction containing  $(\mathbf{x}', \boldsymbol{\omega})$  and the camera. This is also the main reason we chose to swap the camera and the source, since the direct component of the energy emitted from the source is zero except of over a zero measure ray. The final Algorithm 6 is called *adjoint particle tracing*. In the algorithm, we include a caching action at Step 10. This is because, in addition to the image  $I_1$ , we need to estimate directly the light field  $L_1$ . The set of all cached pairs of location and orientation provides us with an approximation of the entire light field  $L_1$ .

In order to estimate the light field  $L_2$ , we perform a stochastic approximation of the single-step propagation operation  $K_k$ , on particles sampled from the cached approximation of  $L_1$ . The resulting new particles from this approximation are stored as an approximation of  $L_2$ . This process is described in Algorithm 7.

Finally, to render the image  $I_3$  from an input light field  $L_2$  using the volume rendering equation, we can use a procedure analogous to Algorithm 6. The only difference is that, instead of sampling from a collimated beam, we now sample from the cached particles produced from Algorithm 7. Moreover, as we only need the image  $I_3$ , no further cache is necessary. This procedure is described in Algorithm 8.

When there is a smooth dielectric interface between the camera and the volume, Algorithms 6 and 8 need to be altered to handle Fresnel refraction, reflection, and total internal reflection (TIR) [Walter et al. 2009]. Among the necessary changes, the steps connecting to the camera need to be changed to capture Fresnel transmission, the scaling of radiance (caused by the compression of solid angle), and the “effective” sensor area  $A$  when observed from inside the medium.

---

**Algorithm 7** Importance sampling for computing  $L_2$ .

```

1:  $C_2 \leftarrow \emptyset$ 
2: Uniformly sample a pair  $(\mathbf{x}_0, \boldsymbol{\omega}_0) \in C_1$ .
3:  $\mathbf{x} \leftarrow \mathbf{x}_0, \boldsymbol{\omega} \leftarrow \boldsymbol{\omega}_0$ .
4:  $\mathbf{x} \leftarrow \mathbf{x} + h\boldsymbol{\omega}$ .
5: Sample  $u$  uniformly in  $(0, 1)$ .
6: if  $u < h(\sigma_{t,k} - \sigma_{s,k})$  then
7:   terminate
8: end if
9: if  $h(\sigma_{t,k} - \sigma_{s,k}) < u < h\sigma_{t,k}$  then
10:  Sample a direction  $\boldsymbol{\psi}$  according to the phase function  $p_k$ .
11:   $\boldsymbol{\omega} \leftarrow \boldsymbol{\psi}$ .
12: end if
13: Cache the particle location  $C_2 \leftarrow C_2 \cup \{(\mathbf{x}, \boldsymbol{\omega})\}$ .

```

---



---

**Algorithm 8** Adjoint particle tracing for computing  $I_3$ .

```

1: Uniformly sample a pair  $(\mathbf{x}_0, \boldsymbol{\omega}_0) \in C_2$ .
2:  $\mathbf{x} \leftarrow \mathbf{x}_0, \boldsymbol{\omega} \leftarrow \boldsymbol{\omega}_0, t \leftarrow 1$ .
3: while true do
4:    $t \leftarrow t \cdot \alpha$ .
5:   Sample  $s$  from pdf  $p(s) = \sigma_t \exp(-\sigma_t s)$ .
6:    $\mathbf{x}' \leftarrow \mathbf{x} + s \cdot \boldsymbol{\omega}$ .
7:   if  $\mathbf{x}' \notin S$  then
8:     break
9:   end if
10:  Let  $\boldsymbol{\psi}_1$  be the direction connecting  $\mathbf{x}'$  and the camera.
11:  Let  $\mathbf{y}_1$  be the intersection of ray  $(\mathbf{x}', \boldsymbol{\psi}_1)$  and the image sensor.
12:   $v_1 \leftarrow t \cdot p(\boldsymbol{\psi}_1^T \boldsymbol{\omega}) \cdot \exp(-\sigma_t \|\mathbf{x}' - \mathbf{y}_1\|) \cdot P_0 c/A$ ,
    where  $c$  is the total number of pixels on the sensor,  $A$  is the
    sensor's surface area, and  $P_0$  is the source power.
13:  Add  $v_1$  to the corresponding pixel on the image sensor.
14:  Sample a direction  $\boldsymbol{\psi}_2$  according to the phase function  $p$ .
15:   $\mathbf{x} \leftarrow \mathbf{x}', \boldsymbol{\omega} \leftarrow \boldsymbol{\psi}_2$ .
16: end while

```

---

## C Operator Theoretic Analysis

In this appendix, we discuss in more detail technical aspects of the operator-theoretic framework for volumetric light transport and its inversion we presented in Sections 3 and 4. Similar or equivalent results to those we present here have been derived in previous literature on operator-theoretic approaches to light transport [Bellman et al. 1975; Bell and Glasstone 1979], for example the boundedness and invertibility of the rendering operator when applied to functions satisfying Hölder conditions [Larsen and Habetler 1973]. Here, we re-derive many of these results, as necessary for the completeness of the operator-theoretic formulation we use.

### C.1 Background

We begin by introducing some definitions and results from the fields of functional analysis, operator theory, and analysis on the sphere, as necessary for our discussion. We draw these from Kato [1966], Yosida [1996], Jörgens and Roach [1982], Lang [1993], and Groemer [1996]. For detailed expositions to these fields, we refer to any of the dedicated mathematical textbooks.

**$\mathcal{L}^p$  spaces.** We will be concerned with the  $\mathcal{L}^p(S \times \mathbb{S}^2)$ ,  $p \in [1, \infty)$  spaces of functions, that is, the set of all functions  $f : S \times \mathbb{S}^2 \mapsto \mathbb{R}$  satisfying

$$\left( \int_S \int_{\mathbb{S}^2} |f(\mathbf{x}, \boldsymbol{\omega})|^p d\mu(\boldsymbol{\omega}) d\mathbf{x} \right)^{\frac{1}{p}} < \infty, \quad (36)$$

where  $S$  a convex subset of the Euclidean space  $\mathbb{R}^3$ ,  $\mathbb{S}^2$  is the two-dimensional unit sphere, and  $\mu$  is the usual spherical Lebesgue mea-

sure on  $\mathbb{S}^2$ . In particular, we will use the spaces  $\mathcal{L}^1(S \times \mathbb{S}^2)$  and  $\mathcal{L}^2(S \times \mathbb{S}^2)$ , for  $p = 1, 2$  respectively. Equipped with the corresponding functional norms,

$$\|f\|_{\mathcal{L}^1(S \times \mathbb{S}^2)} \triangleq \int_S \int_{\mathbb{S}^2} |f(\mathbf{x}, \boldsymbol{\omega})| d\mu(\boldsymbol{\omega}) d\mathbf{x}, \quad (37)$$

$$\|f\|_{\mathcal{L}^2(S \times \mathbb{S}^2)} \triangleq \left( \int_S \int_{\mathbb{S}^2} |f(\mathbf{x}, \boldsymbol{\omega})|^2 d\mu(\boldsymbol{\omega}) d\mathbf{x} \right)^{\frac{1}{2}}. \quad (38)$$

for  $\mathcal{L}^1(S \times \mathbb{S}^2)$  and  $\mathcal{L}^2(S \times \mathbb{S}^2)$  respectively, each of these spaces is a Banach space. Further equipped with the inner product, for all  $f, g \in \mathcal{L}^2(S \times \mathbb{S}^2)$ ,

$$\langle f, g \rangle_{\mathcal{L}^2(S \times \mathbb{S}^2)} \triangleq \int_S \int_{\mathbb{S}^2} f(\mathbf{x}, \boldsymbol{\omega}) g(\mathbf{x}, \boldsymbol{\omega}) d\mu(\boldsymbol{\omega}) d\mathbf{x}, \quad (39)$$

the space  $\mathcal{L}^2(S \times \mathbb{S}^2)$  is a Hilbert space. We will also use the Banach spaces  $\mathcal{L}^1(\mathbb{S}^2)$  and  $\mathcal{L}^1(S)$ , and the Hilbert spaces  $\mathcal{L}^2(\mathbb{S}^2)$  and  $\mathcal{L}^2(S)$ , defined similarly.

For the Hilbert space  $\mathcal{L}^2(\mathbb{S}^2)$ , the following theorem holds.

**Theorem 1.** For any function  $f \in \mathcal{L}^2(\mathbb{S}^2)$ , consider the series  $\sum_{l=0}^{\infty} \sum_{m=-l}^l f_l^m y_l^m$ , where

$$f_l^m = \langle f, y_l^m \rangle_{\mathcal{L}^2(\mathbb{S}^2)}, \quad (40)$$

and  $\{y_l^m, l = 0, \dots, \infty, m = -l, \dots, l\}$  is the set of (real-valued) spherical harmonics. Then, this series converges in the sense of  $\|\cdot\|_{\mathcal{L}^2(\mathbb{S}^2)}$  and its limit is  $f$ ,

$$f = \sum_{l=0}^{\infty} \sum_{m=-l}^l f_l^m y_l^m. \quad (41)$$

The series of Equation (41) is known as the spherical harmonics expansion of  $f$ . The set of spherical harmonics is an orthogonal basis for  $\mathcal{L}^2(\mathbb{S}^2)$ , analogous to the Fourier basis for square-integrable functions on a real interval.

**Bounded operators and operator norm.** An operator  $\mathcal{F} : \mathcal{H} \mapsto \mathcal{H}$ , where  $\mathcal{H}$  some Banach space, is called bounded if there exists  $C \in \mathbb{R}, C > 0$  such that, for all  $f \in \mathcal{H}$

$$\|\mathcal{F}(f)\|_{\mathcal{H}} < C \|f\|_{\mathcal{H}}. \quad (42)$$

We denote by  $\mathcal{B}(\mathcal{H})$  the set of all such operators, and by  $\mathcal{I}$  the unity operator in this set. For each bounded operator  $\mathcal{F}$ , the smallest  $C$  in Equation (42) is called its operator norm induced by the Banach space norm  $\|\cdot\|_{\mathcal{H}}$ , or simply operator norm,

$$\|\mathcal{F}\|_{\text{Op}} \triangleq \sup \left\{ \frac{\|\mathcal{F}(f)\|_{\mathcal{H}}}{\|f\|_{\mathcal{H}}}, f \in \mathcal{H}, f \neq 0 \right\}. \quad (43)$$

The set  $\mathcal{B}(\mathcal{H})$  equipped with the norm  $\|\cdot\|_{\text{Op}}$  is a vector space, with the sum, scalar product, and product operations defined as

$$(\mathcal{F} + \mathcal{G})(f) = \mathcal{F}(f) + \mathcal{G}(f), \quad (44)$$

$$(\mathcal{F})(af) = a\mathcal{F}(f), \quad (45)$$

$$(\mathcal{F}\mathcal{G})(f) = \mathcal{F}(\mathcal{G}(f)), \quad (46)$$

where  $\mathcal{F}, \mathcal{G} \in \mathcal{B}(\mathcal{H})$  and  $a \in \mathbb{R}$ . Then, the operator norm satisfies in particular the following properties with regards to these operations

$$\|\mathcal{F} + \mathcal{G}\|_{\text{Op}} \leq \|\mathcal{F}\|_{\text{Op}} + \|\mathcal{G}\|_{\text{Op}}, \quad (47)$$

$$\|a\mathcal{F}\|_{\text{Op}} = |a| \|\mathcal{F}\|_{\text{Op}}, \quad (48)$$

$$\|\mathcal{F}\mathcal{G}\|_{\text{Op}} \leq \|\mathcal{F}\|_{\text{Op}} \|\mathcal{G}\|_{\text{Op}}. \quad (49)$$

Finally, for any  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$ , we denote by  $B(\mathcal{F}, r)$  the sphere of radius  $r > 0$  and center  $\mathcal{F}$  in  $\mathcal{B}(\mathcal{H})$ ,

$$B(\mathcal{F}, r) = \left\{ \mathcal{G} \in \mathcal{B}(\mathcal{H}), \|\mathcal{F} - \mathcal{G}\|_{\text{Op}} < r \right\}. \quad (50)$$

**Spectrum, resolvent, and spectral radius.** For any  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$ , its spectrum  $\sigma(\mathcal{F})$  is defined as the set of all  $\lambda \in \mathbb{R}$  for which the operator  $(\lambda\mathcal{I} - \mathcal{F})$  does not have a bounded inverse, where the inverse of an operator is defined in the usual way. Then, for any  $\lambda \notin \sigma(\mathcal{F})$ , the resolvent operator  $R(\mathcal{F}, \lambda)$  is defined as

$$R(\mathcal{F}, \lambda) \triangleq (\lambda\mathcal{I} - \mathcal{F})^{-1}. \quad (51)$$

We will in particular be interested in the unit resolvent operator,

$$R(\mathcal{F}) \triangleq R(\mathcal{F}, 1) = (\mathcal{I} - \mathcal{F})^{-1}. \quad (52)$$

In the following, when we say that an operator is “invertible”, we implicitly mean boundedly invertible, that is, that the inverse is bounded. Similarly, when we say that its resolvent (for some  $\lambda$ ) exists, we implicitly mean exists and is bounded.

For any  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$ , its spectral radius  $r(\mathcal{F})$  is defined as

$$r(\mathcal{F}) \triangleq \lim_{n \rightarrow \infty} \|\mathcal{F}^n\|_{\text{Op}}^{\frac{1}{n}}. \quad (53)$$

The definition of the spectral radius is independent of the operator norm used in Equation (53). We will use the following two properties of the spectral radius.

**Theorem 2.** For any  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$ ,

$$r(\mathcal{F}) \leq \|\mathcal{F}\|_{\text{Op}}, \quad (54)$$

$$r(\mathcal{F}) = \sup \{ |\lambda| : \lambda \in \sigma(\mathcal{F}) \}. \quad (55)$$

We will also use the following theorem.

**Theorem 3.** For any  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$  with  $r(\mathcal{F}) < 1$ , the series  $\sum_{n=0}^{\infty} \mathcal{F}^n$  converges absolutely and its limit is equal to the unit resolvent of  $\mathcal{F}$ ,

$$\sum_{j=0}^{\infty} \mathcal{F}^j = R(\mathcal{F}) = (\mathcal{I} - \mathcal{F})^{-1}. \quad (56)$$

with equality defined appropriately.

The series in Equation (56) is often referred to as the Neumann series. That the unit resolvent operator at the right hand side part of Equation (56) exists and is bounded is a consequence of the assumption that  $r(\mathcal{F}) < 1$ , Equation (55), and the definition of spectrum.

**Integral operators and isotropic kernels.** Given any function  $K : \mathbb{S}^2 \times \mathbb{S}^2 \mapsto \mathbb{R}$ , we can define the corresponding integral operator  $\mathcal{C}_K$  on a Banach space  $\mathcal{H}$  of functions on  $\mathbb{S}^2$  by

$$\mathcal{C}_K(f)(\boldsymbol{\omega}) \triangleq \int_{\mathbb{S}^2} K(\boldsymbol{\omega}, \boldsymbol{\psi}) f(\boldsymbol{\psi}) d\mu(\boldsymbol{\psi}), \forall f \in \mathcal{H}. \quad (57)$$

The function  $K$  is called the kernel of the integral operator. When the domain  $\mathcal{H}$  of  $\mathcal{C}_K$  is one of the  $\mathcal{L}^p(\mathbb{S}^2)$  spaces, the following theorem applies.

**Theorem 4.** If for a kernel  $K : \mathbb{S}^2 \times \mathbb{S}^2 \mapsto \mathbb{R}$  there exists a constant  $C > 0$  such that

$$\sup_{\boldsymbol{\omega} \in \mathbb{S}^2} \int_{\mathbb{S}^2} |K(\boldsymbol{\omega}, \boldsymbol{\psi})| d\mu(\boldsymbol{\psi}) < C, \quad (58)$$

$$\sup_{\boldsymbol{\psi} \in \mathbb{S}^2} \int_{\mathbb{S}^2} |K(\boldsymbol{\omega}, \boldsymbol{\psi})| d\mu(\boldsymbol{\omega}) < C, \quad (59)$$



then for any  $f \in \mathcal{L}^p(\mathbb{S}^2)$ ,  $p \in [1, \infty)$ ,

$$\|\mathcal{C}_K(f)\|_{\mathcal{L}^p(\mathbb{S}^2)} \leq C \|f\|_{\mathcal{L}^p(\mathbb{S}^2)}. \quad (60)$$

Equation (60) is also known as (one form of) *Young's inequality*. Equation (60), has the following obvious consequences.

**Lemma 3.** *An operator  $\mathcal{C}_K$  satisfying the conditions of Theorem 4 with domain any of the spaces  $\mathcal{L}^p(\mathbb{S}^2)$ ,  $p \in [1, \infty)$ , has codomain  $\mathcal{L}^p(\mathbb{S}^2)$  ( $\mathcal{C}_K : \mathcal{L}^p(\mathbb{S}^2) \mapsto \mathcal{L}^p(\mathbb{S}^2)$ ), is in  $\mathcal{B}(\mathcal{L}^p(\mathbb{S}^2))$  (is bounded), and its corresponding norm is  $\|\mathcal{C}_K\|_{\text{op}} \leq C$ .*

A kernel  $K$  is called *isotropic* when it is a function of only the spherical distance between  $\omega$  and  $\psi$ ; equivalently, this means that  $K$  can be written in the form

$$K(\omega, \psi) = \kappa(\omega^T \psi), \quad \forall (\omega, \psi) \in \mathbb{S}^2 \times \mathbb{S}^2, \quad (61)$$

for some function  $\kappa : [-1, 1] \mapsto \mathbb{R}$  that is called the *profile* of  $K$ . The following theorem applies to integral operators corresponding to such kernels.

**Theorem 5.** *Let  $K$  be an isotropic kernel for which its profile  $\kappa$  is integrable,*

$$\int_{-1}^1 |\kappa(t)| dt < \infty. \quad (62)$$

*Then, for the corresponding integral operator  $\mathcal{C}_K$  and any square-integrable function  $f \in \mathcal{L}^2(\mathbb{S}^2)$ , the following holds*

$$\mathcal{C}_K(f)(\omega) = \sum_{l=0}^{\infty} C_{1\kappa l} \sum_{m=-l}^l f_l^m y_l^m(\omega). \quad (63)$$

where

$$\kappa_l = \int_{-1}^1 \kappa(t) P_l(t) dt, \quad l \in \{0, \dots, \infty\} \quad (64)$$

are the coefficients of the expansion of  $\kappa$  in terms of Legendre polynomials  $\{P_l(t), t \in [-1, 1], l = 0, \dots, \infty\}$ ;  $f_l^m$ ,  $l \in \{0, \dots, \infty\}$ ,  $m \in \{-l, \dots, l\}$  are the coefficients of the spherical harmonics expansion of  $f$  (Equation (41)); and  $\{C_{1\kappa l}, l = 0, \dots, \infty\}$  are constants independent of  $\kappa$  and  $f$ .

Theorem 5 is known as the *Funk-Hecke theorem*. The integral operator  $\mathcal{C}_K$  for an isotropic kernel  $K$  is often described as an (isotropic) *spherical convolution*, and Theorem 5 is seen as the analogous of the convolution theorem for functions on  $\mathbb{R}$ . Theorem 5 is well known in computer graphics, where it has been used, for instance, for the problems of surface light transport and normal map filtering [Sloan et al. 2002; Ramamoorthi and Hanrahan 2001; Han et al. 2007; Basri and Jacobs 2003]. In the remaining of this section, we use the kernel  $K$  and its profile  $\kappa$  interchangeably, and write directly  $K(\omega^T \psi)$  for convenience.

## C.2 Volume Light Transport Operators

We continue to study the various operators we defined in Section 3.1. In our analysis, we assume that light fields  $L$  are functions in either the Banach space  $\mathcal{L}^1(S \times \mathbb{S}^2)$  or the Hilbert space  $\mathcal{L}^2(S \times \mathbb{S}^2)$ , as is usual in functional analytic treatments of light transport [Arvo 1995; Veach 1997], and establish results for both cases.

We first introduce some notation. We define the following linear operators in terms of the material parameters  $k = \{\sigma_t, \sigma_s, p(\theta)\}$ ,

$$\mathcal{C}_p(f)(\omega) \triangleq \int_{\mathbb{S}^2} p(\omega^T \psi) f(\psi) d\mu(\psi), \quad (65)$$

$$\mathcal{A}_k(f)(\omega) \triangleq ((1 - h\sigma_t)\mathcal{I} + h\sigma_s \mathcal{C}_p)(f)(\omega), \quad (66)$$

$$\mathcal{T}_{h\omega}(g)(\mathbf{x}) \triangleq g(\mathbf{x} - h\omega), \quad (67)$$

where  $\mathcal{C}_p$  and  $\mathcal{A}_k$  operate on functions defined on  $\mathbb{S}^2$ , and  $\mathcal{T}_{h\omega}$  operates on functions defined on the spatial domain  $\mathbb{R}^3$ . Then, the single-step propagation operator of Equation (8) can be expressed as their composition

$$\mathcal{K}_k(L)(\mathbf{x}, \omega) = \mathcal{A}_k \mathcal{T}_{h\omega}(L)(\mathbf{x}, \omega) \quad (68)$$

**Phase function and its integral operator.** The phase function can, in its most general form, be any function  $P : \mathbb{S}^2 \times \mathbb{S}^2 \mapsto \mathbb{R}^+$  that satisfies appropriate normalization and reciprocity conditions [Jakob et al. 2010]. Traditionally though, the phase function is restricted to be invariant to rotations of the incident direction and cylindrically symmetric. Under this assumption, the phase function is an isotropic kernel,

$$P(\omega, \psi) = p(\omega \cdot \psi) \quad (69)$$

with some profile  $p : [-1, 1] \mapsto \mathbb{R}^+$  that is restricted to take only positive values. Any function of this form obviously satisfies reciprocity in terms of their two arguments; and therefore, to be a valid phase function, it only needs additionally to satisfy the normalization constraint

$$\int_{\mathbb{S}^2} p(\omega \cdot \psi) d\mu(\psi) = 1, \quad \forall \omega \in \mathbb{S}^2. \quad (70)$$

This condition can be written equivalently in the following two forms (see, for instance, Lemma 1.3.1, page 9 of Groemer [1996]),

$$2\pi \int_{-1}^1 p(t) dt = 1, \quad (71)$$

$$2\pi \int_0^\pi p(\cos(\theta)) \sin(\theta) d\theta = 1, \quad (72)$$

where in Equation (72) we used  $\theta = \arccos(t)$ . In an abuse of notation,  $p(\theta)$  is often used instead of  $p(\cos(\theta))$ ; we also use this convention, which leads us to the normalization condition we showed in Equation (2).

For a material with phase function  $p(\theta)$ , we consider first the operator  $\mathcal{C}_p$  of Equation (65), as applied to functions in  $\mathcal{L}^1(\mathbb{S}^2)$  or  $\mathcal{L}^2(\mathbb{S}^2)$ . As can be seen immediately using the terminology we established in Section C.1, this is an integral operator of the form of Equation (57) for the kernel corresponding to the material phase function. Furthermore, from the normalization condition of Equation (70), it is obvious that this kernel satisfies the conditions (58)-(59) for Theorem 4, with  $C = 1$ . Therefore, from Lemma 3, the operator  $\mathcal{C}_p$  is in both  $\mathcal{B}(\mathcal{L}^1(\mathbb{S}^2))$  and  $\mathcal{B}(\mathcal{L}^2(\mathbb{S}^2))$  and has norm

$$\|\mathcal{C}_p\|_{\text{op}} \leq 1 \quad (73)$$

**Boundedness of single-step propagation operator.** For a material  $k = \sigma_t, \sigma_s, p(\theta)$ , we consider now the angular part of its single-step propagation operator,  $\mathcal{A}_k$  defined in Equation (66), as applied to functions in  $\mathcal{L}^1(\mathbb{S}^2)$  or  $\mathcal{L}^2(\mathbb{S}^2)$ . From Equations (47)-(48), we have

$$\|\mathcal{A}_k\|_{\text{op}} \leq (1 - h\sigma_t) \|\mathcal{I}\|_{\text{op}} + h\sigma_s \|\mathcal{C}_p\|_{\text{op}} \leq (1 - h\sigma_t) + h\sigma_s \quad (74)$$

$$= 1 - h\sigma_a, \quad (75)$$

where in Equation (74) we used the fact that the operator norm of the unity operator is trivially equal to one and the bound (73) we derived, and in Equation (75) we used  $\sigma_a = \sigma_t - \sigma_s$ .

Both Equations (73) and (75) are derived for the case of the  $\mathcal{L}^1(\mathbb{S}^2)$  and  $\mathcal{L}^2(\mathbb{S}^2)$  domains (functions of direction only). However,

they can be easily extended to the case of the  $\mathcal{L}^1(S \times \mathbb{S}^2)$  and  $\mathcal{L}^2(S \times \mathbb{S}^2)$  (functions of both space and direction) that light fields reside in by a simple application of Fubini's theorem.

Finally, for the full single-step propagation operator  $\mathcal{K}_k$  defined in Equation (5), as applied to functions in  $\mathcal{L}^1(S \times \mathbb{S}^2)$  or  $\mathcal{L}^2(S \times \mathbb{S}^2)$ , using Equation (49) we have

$$\|\mathcal{K}_k\|_{\text{Op}} \leq \|\mathcal{A}_k\|_{\text{Op}} \|\mathcal{T}_{h\omega}\|_{\text{Op}} \leq 1 - h\sigma_a, \quad (76)$$

where we have used the fact that  $\|\mathcal{T}_{h\omega}\|_{\text{Op}} = 1$ . Therefore, we have proved that the single scattering operator  $\mathcal{K}_k$  for material  $k$  is in both  $\mathcal{B}(\mathcal{L}^1(S \times \mathbb{S}^2))$  and  $\mathcal{B}(\mathcal{L}^2(S \times \mathbb{S}^2))$ .

**Existence of rendering operator.** We now turn our attention to the rendering operator  $\mathcal{R}_k$  defined in Equation (8), and we observe that it is equal by definition to the unit resolvent  $R(\mathcal{K}_k)$ , as defined in Equation (52), of the single scattering operator.

From Equation (54) and the bound of Equation (76) we derived earlier, we have that

$$r(\mathcal{K}_k) \leq 1 - h\sigma_a. \quad (77)$$

For any absorbing material  $k$ ,  $\sigma_a > 0$ , the above inequality implies that  $r(\mathcal{K}_k) < 1$ . Consequently, from Theorem 3, we have that the rendering operator  $\mathcal{R}_k$  for that material exists, is bounded (is in both  $\mathcal{B}(\mathcal{L}^1(S \times \mathbb{S}^2))$  and  $\mathcal{B}(\mathcal{L}^2(S \times \mathbb{S}^2))$ ), and can be represented in terms of the Neumann series, as in the second equality in Equation (8).

**Dictionary of materials.** By using Lemma 1 and Equations (12)-(13) and (15), we can see that the above results directly extend to the case of a dictionary of materials. Specifically, as long as the bulk absorption coefficient of the mixture material, as given by Equations (12), is non-zero, then the rendering operator  $\mathcal{R}(\boldsymbol{\pi})$  exist and is bounded. This can be achieved either by having a purely absorbing ( $\sigma_t > 0$  and  $\sigma_s = 0$ ) material in the dictionary that is assigned a non-zero mixture weight, or by using a dictionary where all of the atoms have non-zero absorption.

### C.3 Differentiation of Rendering Operator

In Section 4, we derived the expression of Equation (19) for the gradient of the objective function  $E(\boldsymbol{\pi})$  of the appearance matching optimization problem of Equation (14). In the derivation, we used Lemma 2 to differentiate the rendering operator  $\mathcal{R}(\boldsymbol{\pi})$  with respect to the components of the weight vector  $\boldsymbol{\pi}$ . In this appendix, we provide the precise technical formulation of the lemma and its proof, as well as show the full derivation of Equation (19).

We will use two lemmata. The first follows from Theorem 3.11, page 210 of Kato [1966].

**Lemma 4.** *For a Banach space  $\mathcal{H}$ , if for a bounded operator  $\mathcal{F} \in \mathcal{B}(\mathcal{H})$  its unit resolvent  $R(\mathcal{F})$  exists, then there exists some  $r > 0$  such that, for all operators  $\mathcal{G}$  in the sphere  $B(\mathcal{F}, r)$ , their unit resolvent  $R(\mathcal{G})$  exists. Furthermore, the unit resolvent  $R(\mathcal{G})$ , as a function of  $\mathcal{G}$ , is continuous in  $B(\mathcal{F}, r)$ , with continuity defined in the sense of  $\|\cdot\|_{\text{Op}}$ .*

The second lemma follows from the *second resolvent equation* (see for instance page 65 of Jörgens and Roach [Jörgens and Roach 1982]).

**Lemma 5.** *For a Banach space  $\mathcal{H}$ , if for two bounded operators  $\mathcal{F}, \mathcal{G} \in \mathcal{B}(\mathcal{H})$  their unit resolvents  $R(\mathcal{F})$  and  $R(\mathcal{G})$  exist, then*

$$R(\mathcal{F}) - R(\mathcal{G}) = R(\mathcal{F})(\mathcal{F} - \mathcal{G})R(\mathcal{G}). \quad (78)$$

We now restate and prove Lemma 2.

**Lemma 6.** *For a Banach space  $\mathcal{H}$ , let the operator  $\mathcal{F}(\boldsymbol{\pi})$  for any weight vector  $\boldsymbol{\pi} \in \mathbb{R}^N$  be defined as  $\mathcal{F}(\boldsymbol{\pi}) \triangleq \sum_{n=1}^N \pi_n \mathcal{F}_n$ , where  $\{\mathcal{F}_n \in \mathcal{B}(\mathcal{H}), n = 1, \dots, N\}$  is a set of bounded linear operators. Then, if its unit resolvent  $R(\mathcal{F}(\boldsymbol{\pi}))$  exists, the following differentiation rule holds*

$$\frac{\partial}{\partial \pi_n} R(\mathcal{F}(\boldsymbol{\pi})) = R(\mathcal{F}(\boldsymbol{\pi})) \mathcal{F}_n R(\mathcal{F}(\boldsymbol{\pi})). \quad (79)$$

*Proof.* If we denote by  $\{\mathbf{e}_n \in \mathbb{R}^N, n = 1, \dots, N\}$  the set of standard basis vectors in  $\mathbb{R}^N$ , from the definition of  $\mathcal{F}(\boldsymbol{\pi})$  we have for every  $\varepsilon \in \mathbb{R}$ ,

$$\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n) = \mathcal{F}(\boldsymbol{\pi}) + \varepsilon \mathcal{F}_n \Rightarrow \quad (80)$$

$$\|\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n) - \mathcal{F}(\boldsymbol{\pi})\|_{\text{Op}} = |\varepsilon| \|\mathcal{F}_n\|_{\text{Op}}, \quad (81)$$

where in (81) we used Equation (48). As  $\mathcal{F}(\boldsymbol{\pi}), R(\mathcal{F}(\boldsymbol{\pi})) \in \mathcal{B}(\mathcal{H})$ , the conditions of Lemma 4 are satisfied. If  $r$  is as in that lemma, and given that  $\|\mathcal{F}_n\|_{\text{Op}}$  is finite from the boundedness assumption, then for all  $|\varepsilon|$  such that

$$|\varepsilon| < \frac{r}{\|\mathcal{F}_n\|_{\text{Op}}}, \quad (82)$$

it follows from Equation (81) that  $\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n) \in B(\mathcal{F}(\boldsymbol{\pi}), r)$ , and from Lemma 4 that the unit resolvent  $R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n))$  exists. Also, for any such  $\varepsilon$ , the conditions of Lemma 5 are satisfied for operators  $\mathcal{F}(\boldsymbol{\pi})$  and  $\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n)$ , therefore we have

$$\begin{aligned} \Delta_n(\varepsilon) &\triangleq \frac{R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n)) - R(\mathcal{F}(\boldsymbol{\pi}))}{\varepsilon} \\ &\stackrel{(78)}{=} \frac{R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n))(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n) - \mathcal{F}(\boldsymbol{\pi}))R(\mathcal{F}(\boldsymbol{\pi}))}{\varepsilon} \\ &\stackrel{(80)}{=} \frac{R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n))(\varepsilon \mathcal{F}_{k_n})R(\mathcal{F}(\boldsymbol{\pi}))}{\varepsilon} \\ &= R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n)) \mathcal{F}_n R(\mathcal{F}(\boldsymbol{\pi})). \end{aligned} \quad (83)$$

When  $\varepsilon \rightarrow 0$ , from Equation (81) we have that

$$\lim_{\varepsilon \rightarrow 0} \mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n) = \mathcal{F}(\boldsymbol{\pi}), \quad (84)$$

where the convergence is in the sense of  $\|\cdot\|_{\text{Op}}$ . As we established earlier, for all  $|\varepsilon|$  small enough to satisfy Equation (82), Lemma 4 applies for  $\mathcal{F}(\boldsymbol{\pi})$  and  $\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n)$  is in the ball defined by the lemma. Then, using now the continuity statement of the lemma with Equation (84), it follows that

$$\lim_{\varepsilon \rightarrow 0} R(\mathcal{F}(\boldsymbol{\pi} + \varepsilon \mathbf{e}_n)) = R(\mathcal{F}(\boldsymbol{\pi}))^{-1}, \quad (85)$$

and therefore, combining with Equation (83),

$$\lim_{\varepsilon \rightarrow 0} \Delta(\varepsilon) = R(\mathcal{F}(\boldsymbol{\pi})) \mathcal{F}_{k_n} R(\mathcal{F}(\boldsymbol{\pi})), \quad (86)$$

as desired.  $\square$

We consider now the dictionary single-step propagation and rendering operators,  $\mathcal{K}(\boldsymbol{\pi})$  and  $\mathcal{R}(\boldsymbol{\pi}) = R(\mathcal{K}(\boldsymbol{\pi})) = (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1}$ , respectively. As we established at the end of the previous subsection, under the condition that the equivalent bulk material  $k(\boldsymbol{\pi})$  has non-zero absorption, both of these operators are in both  $\mathcal{B}(\mathcal{L}^1(S \times \mathbb{S}^2))$  and  $\mathcal{B}(\mathcal{L}^2(S \times \mathbb{S}^2))$ . Therefore, the conditions

of Lemma 6 are satisfied. Using it, we can derive Equation (19) as follows

$$\begin{aligned} \frac{\partial}{\partial \pi_n} E(\boldsymbol{\pi}) &= \sum_{m=1}^M w_m \frac{\partial}{\partial \pi_n} (\mathcal{S}^m (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} L_i^m - \bar{I}^m)^2 \\ &= \sum_{m=1}^M 2w_m (\mathcal{S}^m (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} L_i^m - \bar{I}^m) \\ &\quad \cdot \mathcal{S}^m \left( \frac{\partial}{\partial \pi_n} (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} L_i^m \right) \\ &\stackrel{(18)}{=} \sum_{m=1}^M 2w_m (\mathcal{S}^m (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} L_i^m - \bar{I}^m) \\ &\quad \cdot \mathcal{S}^m ((\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} \mathcal{K}_{k_n} (\mathcal{I} - \mathcal{K}(\boldsymbol{\pi}))^{-1} L_i^m), \end{aligned} \quad (87)$$

where in using Equation (79), we expanded the unit resolvent to its explicit expression.

#### C.4 Scattering Parameter Recovery and Illumination

We start this section by stating the following lemma.

**Lemma 7.** *For a Banach space  $\mathcal{H}$ , if for an operator  $\mathcal{F}$  its unit resolvent  $R(\mathcal{F})$  exists, then*

$$R(\mathcal{F}) = \mathcal{I} + R(\mathcal{F})\mathcal{F}. \quad (88)$$

Its validity can be seen trivially by using the definition of unit resolvent from Equation (52) in Equation (88) (this lemma is analogous to a simplified version of the *matrix inversion lemma* known for finite dimensional matrices).

For the remaining of this section, we constrain our analysis to light fields in the space  $\mathcal{L}^2(S \times \mathbb{S}^2)$ . We also assume that we have a material  $k$  satisfying the absorption condition we derived in Section C.2, so that both the single-step propagation and rendering operators,  $\mathcal{K}_k$  and  $\mathcal{R}_k$  respectively, are in  $\mathcal{B}(\mathcal{L}^2(S \times \mathbb{S}^2))$ . As established by Equation (68),  $\mathcal{K}_k$  can be written as the tensor product

$$\mathcal{K}_k(L)(\mathbf{x}, \boldsymbol{\omega}) = \mathcal{T}_{h\boldsymbol{\omega}} \mathcal{A}_k(L)(\mathbf{x}, \boldsymbol{\omega}), \quad (89)$$

of the direction-dependent and independent of the material bulk parameters operator  $\mathcal{T}_{h\boldsymbol{\omega}}$  applying only on the spatial coordinate of  $L$ , and the dependent on the material parameters operator  $\mathcal{A}_k$  applying only on the angular coordinate of  $L$ . Using this decomposition and Equation (88), we obtain for the rendering operator  $\mathcal{R}_k$

$$\begin{aligned} \mathcal{R}_k(L)(\mathbf{x}, \boldsymbol{\omega}) &\triangleq (\mathcal{I} - \mathcal{K}_k)^{-1}(L)(\mathbf{x}, \boldsymbol{\omega}) \\ &= \mathcal{I}(L)(\mathbf{x}, \boldsymbol{\omega}) + \mathcal{R}_k \mathcal{T}_{h\boldsymbol{\omega}} \mathcal{A}_k(L)(\mathbf{x}, \boldsymbol{\omega}). \end{aligned} \quad (90)$$

We now turn our attention to the angular domain operator  $\mathcal{A}_k$ . This operator is equal to the weighted sum of the unity operator and the integral operator  $\mathcal{C}_p$ , both applying on the space  $\mathcal{L}^2(\mathbb{S}^2)$ . From the discussion at the beginning of Section C.2, we see immediately that the operator  $\mathcal{C}_p$  satisfies all of the conditions of Theorem 5, and therefore we can write

$$\mathcal{C}_p(f)(\boldsymbol{\omega}) = \sum_{l=0}^{\infty} \sum_{m=-l}^l C_l p_l f_l^m y_l^m(\boldsymbol{\omega}) \text{ a.e.}, \quad (91)$$

where  $\{p_l, l = 0, \dots, \infty\}$  is the expansion of the phase function profile in terms of Legendre polynomials. Furthermore, from Theorem 1, we can write

$$\mathcal{I}(f)(\boldsymbol{\omega}) = \sum_{l=0}^{\infty} \sum_{m=-l}^l f_l^m y_l^m(\boldsymbol{\omega}) \text{ a.e.} \quad (92)$$

Using Equations (91) and (92) with the definition of  $\mathcal{A}_k(\boldsymbol{\pi})$  in Equation (66), we obtain

$$\mathcal{A}_k(f)(\boldsymbol{\omega}) = \sum_{l=0}^{\infty} \sum_{m=-l}^l w_l f_l^m y_l^m(\boldsymbol{\omega}) \text{ a.e.} \quad (93)$$

where

$$w_l = 1 - h\sigma_t + h\sigma_s p_l, \quad l = 0, \dots, \infty. \quad (94)$$

By combining Equations (93) and (90), we obtain for the rendering operator  $\mathcal{R}_k$

$$\begin{aligned} \mathcal{R}_k(L)(\mathbf{x}, \boldsymbol{\omega}) &= \mathcal{I}(L)(\mathbf{x}, \boldsymbol{\omega}) \\ &\quad + \mathcal{R}_k \mathcal{T}_{h\boldsymbol{\omega}} \sum_{l=1}^{\infty} \sum_{m=-l}^l w_l L(\mathbf{x})_l^m y_l^m(\boldsymbol{\omega}) \text{ a.e.}, \end{aligned} \quad (95)$$

where for each  $\mathbf{x} \in S$ ,  $\{L(\mathbf{x})_l^m\}$  is the spherical harmonics expansion of  $L(\mathbf{x}, \boldsymbol{\omega})$ ,  $\boldsymbol{\omega} \in \mathbb{S}^2$ .

The final result of the above derivation, Equation (95), shows that the rendering operation  $\mathcal{R}_k$  at a first stage performs a frequency decomposition and filtering of any input light field  $L$ , with the filtering weights being related to the material parameters through Equation (94). It is also easy to show that this result applies directly to the case of a material dictionary and corresponding single-step propagation and rendering operators,  $\mathcal{K}(\boldsymbol{\pi})$  and  $\mathcal{R}(\boldsymbol{\pi})$  respectively. Indeed, we see immediately from Equation (94) that the frequency terms  $w_l$  of the decomposition in Equation (95) are linear mixtures with weights  $\boldsymbol{\pi}$  of the corresponding frequency terms for each of the individual dictionary materials.

Equation (95) provides us with the following insight: the light sources we use in an inverse volume rendering setup should be designed in a way such that the corresponding input light field  $L_i(\mathbf{x}, \boldsymbol{\omega})$  is “broadband” in the angular domain, so that as few of the frequency terms  $L(\mathbf{x})_l^m$  in Equation (95) as possible are zero (or, intuitively, as fewer “columns” of the rendering operator are cancelled out). This implies that the optimal lighting conditions for inverse volume rendering are functions which are Dirac delta in the angular domain, that is, collimated light sources.

Concluding this section, we mention that the above derivation can be applied almost identically to the volume rendering formulation of Appendix A. This can be seen by observing that a tensor-product expression analogous to that of Equation (89) can also be written for the single-scattering operator  $\mathcal{B}_k$ , by replacing  $\mathcal{T}_{h\boldsymbol{\omega}}$  with the spatial domain operator

$$\mathcal{T}_{V, \sigma_t, \boldsymbol{\omega}}(f)(\mathbf{x}) = \int_0^{r_{\partial S}(\mathbf{x}, \boldsymbol{\omega})} \exp(-\sigma_t r') f(\mathbf{x} - r'\boldsymbol{\omega}) dr'. \quad (96)$$

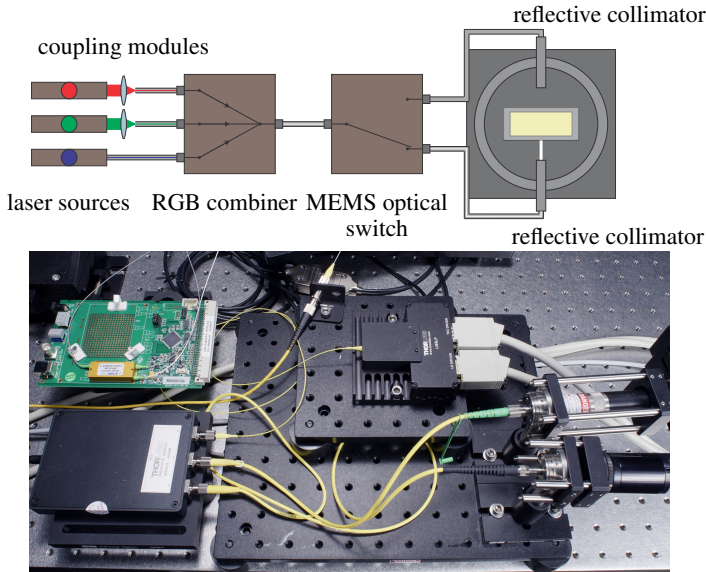
The rest of the derivation then follows by replacing Equations (6) and (8) with their counterparts, Equations (26) and (25) respectively.

## D Implementation and Calibration

We provide details about our implementation of the proposed acquisition setup, as shown in Figure 4, as well as the necessary calibration procedures.

### D.1 Implementation

**Imaging system.** We use a CRi Nuance MSI-FX hyperspectral camera. The camera uses an integrated liquid crystal tunable filter



**Figure 11:** Light generation and control. Top: schematic; bottom: implementation.

that can be tuned to narrow wavelength bands of full-width-half-maximum of approximately 20 nm, and centered at any wavelength  $\lambda \in [420 \text{ nm } 720 \text{ nm}]$ . The camera is equipped with a  $1392 \times 1040$  pixel 12-bit grayscale sensor.

The camera is equipped with a Nikon 105mm f/2.8D AF Micro-Nikkor macro lens, which we focus at its closest working distance for maximum magnification. The lens is mounted through an F-to-C mount that includes an apochromatic optical element. Overall, this configuration produces an effective reproduction ratio of 1 : 1.60, field of view of  $14.25 \text{ mm} \times 10.75 \text{ mm}$ , and subtended angle of  $4^\circ$ .

A large depth of field is necessary in order for a sufficient part of the glass cells to remain in focus when imaging them at large viewing angles, and across all wavelengths (chromatic aberration means that the in-focus part of the field of view shifts as wavelength changes). For this reason, we use an  $f/16$  aperture setting in all of our measurements. We avoided using smaller apertures, as that resulted in very noticeable diffraction artifacts.

**Light generation and control.** We use three separate continuous-wave laser sources for each of the three wavelengths we use for imaging. For the blue wavelength, 488 nm, we use a laser diode pigtailed to a fiber cable. For the green, 532 nm, and red, 635 nm, wavelengths, we use separate laser modules that output collimated beams, which we then couple into fiber cables using two micropositioner-and-lens modules. We use single-mode, non-polarization preserving 460-HP fiber cables in all of our setup.

The fiber-coupled outputs of our three laser sources are combined into multichromatic white light coupled into a single fiber using an off-the-shelf RGB combiner designed for the three wavelengths of our sources. The output of the RGB combiner is connected through a fiber cable to the input of a  $1 \times 2$  computer-controlled optical MEMS switch. The outputs of the switch are connected through fiber cables to two collimator modules. For collimation, we use reflective collimators, each employing a  $90^\circ$  off-axis parabolic mirror element to achieve achromatic collimation.

The entire optical circuit is shown in Figure 11. Our use of coherent laser sources is motivated by the need to simultaneously achieve: 1) thin and very-well collimated beams that we can easily calibrate and

simulate; and 2) high output power to enable us to measure optically thick materials. In our setup, we produce beams of diameter 1 mm, divergence of  $0.05^\circ$ , and power of approximately 1 mW at each of the three wavelengths we use.

**Mechanical control.** We use two computer-controlled rotation stages in our acquisition setup, as shown in Figure 4. The bottom stage is used to rotate both the material sample and collimator configuration relative to the camera, thus controlling the viewing direction  $\theta_v$ . It has an angular resolution of  $0.001^\circ$ , and produces rotations repeatable within  $0.02^\circ$ . It is important to note that repeatability of the bottom rotation stage is not critical: as discussed in the following subsection, its position is geometrically calibrated to within subpixel error after each rotation.

The top rotation stage is used to rotate the two collimators relative to the material sample, thus controlling the lighting directions  $\theta_f, \theta_b$ . This stage has the same resolution of  $0.001^\circ$ , but a much higher repeatability, producing rotations repeatable within  $0.003^\circ$ , which we have measured to correspond to subpixel error. Repeatability of this stage is important, as the positions of the collimators are geometrically calibrated only once relative to a fixed plane in the 3D scene, and their locations relative to that plane are afterwards assumed known.

Finally, the platform the material sample is placed on is mounted on a computer-controlled  $XY$ -linear translation stage, that is used only during the calibration of the collimator positions, as described in the following. Those produce translations of the sample relative to the rest of the setup at a linear resolution of  $0.3 \mu\text{m}$  and repeatable within  $1.5 \mu\text{m}$ . The repeatability of this stage is also not critical: as discussed in the following subsection, its position is geometrically calibrated to within subpixel error after every translation.

**Geometry.** To create material samples with very precise geometry, we cast them into rectangular glass spectrophotometer cells. The cells are manufactured from B270 borosilicate crown optical glass, using a fully fused method. This process results in glass cells with the following specifications: surfaces parallel to less than  $0.05^\circ$ ; surface flatness less than 4 Newton fringes; dimension tolerances less than  $10 \mu\text{m}$ .

## D.2 Calibration

**Geometric calibration.** For the geometric calibration of our capture setup, we use two planar targets, one opaque and one a thin transparency, having a square grid of circular control points of diameter 0.25 mm printed on them with micrometer accuracy. The calibration procedure then is performed in three stages. First, we capture a set of images of the opaque target, at different orientations and positions. Then, we fix the opaque target on the center stage of the setup, where the sample is normally located. We use a pair of mechanized translation stages to perform translations of the target, parallel to its surface normal. For each such translation, we capture images of the target, first illuminated by ambient light, and then by the two light sources at each of their three rotations (top rotation stage) relative to the center stage. Finally, we replace the opaque target with the cell containing the material sample, with the transparent target adjacent to the cell surface facing the camera. Each time the bottom rotation stage is moved, we capture an image of the sample under ambient light with the target present, as well as images of the sample without the target under laser illumination (which constitute our measurements).

The set of target images are then processed using the algorithm by Heikkila [2000]. This algorithm allows us to recover the intrinsic parameters of the camera, as well as the extrinsic parameters (relative locations of the planar target in the camera-coordinate system)

for each target image. From the images of the opaque target under laser illumination and for multiple parallel translations, we can fit a straight line that corresponds to the direction of the corresponding light source. Finally, from the images of the transparent target, we can calibrate the location of the frontal surface of the cell relative to the camera and the rest of the setup.

We performed the calibration of the sources and sample every time we captured a new material. The source direction, controlled by the top (high-repeatability) rotation stage controlling the orientation of the sources relative to the sample, were calibrated once per capture session, for a fixed sample position. The location of the sample relative to the entire setup was calibrated each time the bottom stage was rotated.

**Index of refraction.** To measure the index of refraction, we first rotate the light source so that it points directly into the camera. Then, we place a glass sample in the middle of the optical path between the source and the camera. The positions of the source and sample relative to the camera are calibrated as described above. By measuring the displacement of the peak intensity before and after the placement of the sample, and knowing the index of refraction of the glass cell, we can estimate the index of refraction of the material using simple geometric optics.

The above procedure is exactly accurate only under the assumption that a material is transparent. For scattering materials, the location of the peak intensity also depends on the scattering parameters of the material. However, if the sample used in the above process is sufficiently thin relative to the optical thickness of the material, the above procedure will still produce accurate estimates. In our experiments, we used cells of width 1 mm for the measurement of the index of refraction. From simulations, we verified that for the range of materials we measure ( $\sigma_t < 200 \text{ mm}^{-1}$ ), the index of refraction estimates we obtain are always within 0.1 of the true value.

**High-dynamic range imaging.** For all of our measurements, we capture a stack of images using 19 exposure times, equally spaced in a logarithmic scale from 0.1 ms to 26 s. For exposure times smaller than 0.5 s, we average across 10 images in order to reduce the effect of noise caused by Brownian motion in the scattering medium. We then combine the raw, 12-bit images from different exposure times into a single, high-dynamic range (HDR) image. For this, we use a variance-based weighting scheme [Hasinoff et al. 2010], which we found to perform significantly better than the usual linear weighting. In the conversion, we assume a linear response curve for the camera sensor. We validated the accuracy of this assumption, by capturing images of a planar white diffuse target (Spectralon) under white illumination at different exposure times and comparing the recorded intensities.

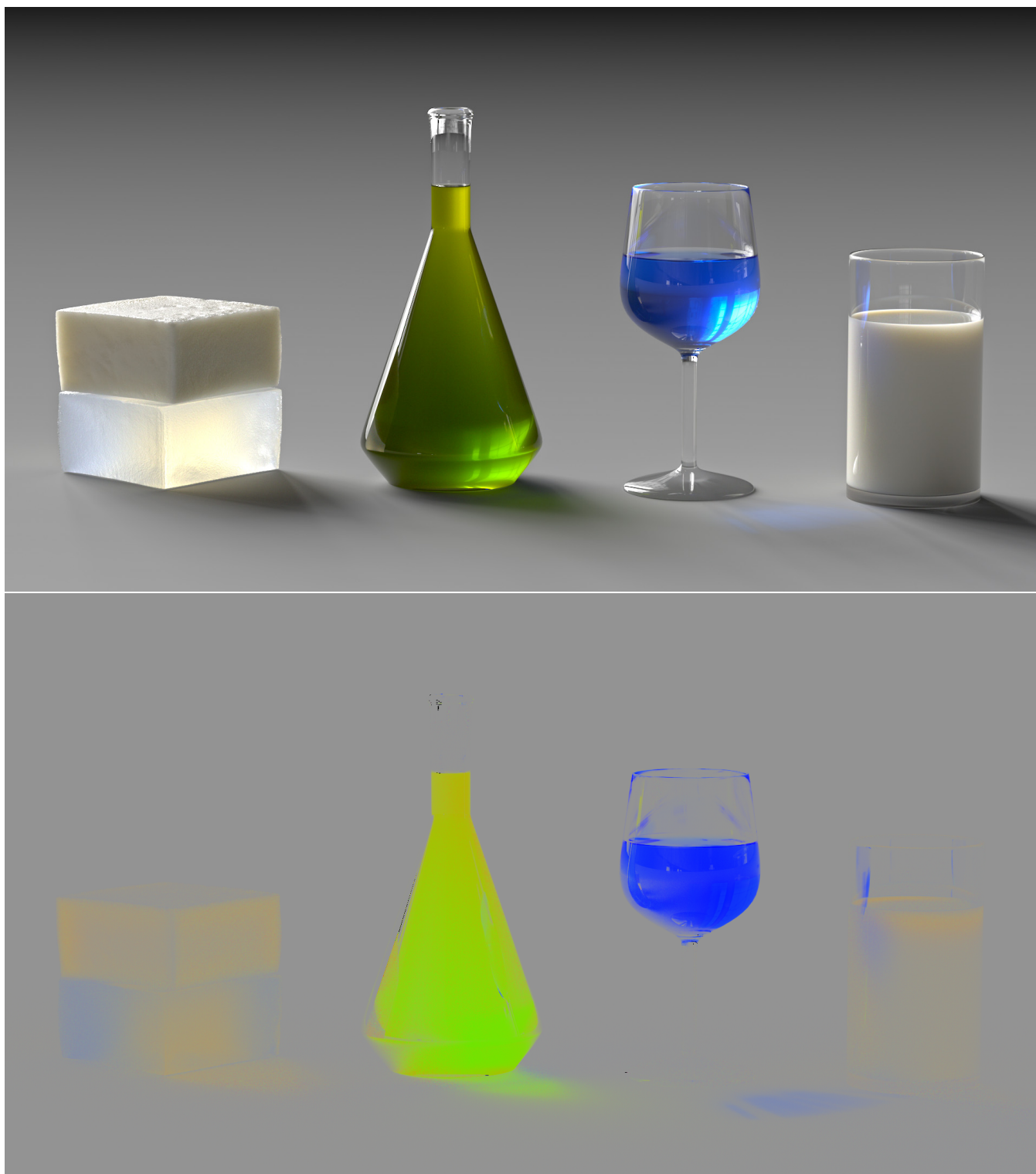
**Color calibration.** The parameters we measure correspond to three nearly-monochromatic wavelength bands, and not to any true linear color space. To approximate standard linear RGB images, we apply a fixed  $3 \times 3$  linear color transform to the rendered output produced from our parameters. To estimate the color transform to be applied, we use our imaging system to capture images of a Macbeth colorchecker target under two illuminations: a 32-channel hyperspectral cube under broadband white light; and a 3-channel image under the trichromatic light produced by our light generation system. We white balance the hyperspectral cube captured under broadband white light to match D65 illumination, and use it to render an RGB image of the colorchecker. Then, we obtain the  $3 \times 3$  scaling matrix  $\mathbf{A}$  for matching the 3-channel image of the colorchecker under trichromatic light to the RGB image under D65 light, by solving a linear least-squares problem. The exact  $3 \times 3$  matrix is available at the project website.

## E Rendering of Measured Materials

In Figure 12, we show a high-resolution version of the rendered image of measured materials under natural lighting of Figure 1-right. We also show a version of the same image where all RGB vectors are normalized to unit norm, in order to highlight the color variations in the various materials.

## References

- ANTYUFEEV, V. 2000. *Monte Carlo method for solving inverse problems of radiation transfer*, vol. 20. Inverse and Ill-Posed Problems Series, V.S.P. International Science.
- ARVO, J. 1995. *Analytic methods for simulated light transport*. PhD thesis, PhD thesis, Yale University.
- BAL, G. 2009. Inverse transport theory and applications. *Inverse Problems* 25, 5.
- BASRI, R., AND JACOBS, D. W. 2003. Lambertian reflectance and linear subspaces. *IEEE Transactions of Pattern Analysis and Machine Intelligence* 25, 2.
- BELL, G. I., AND GLASSTONE, S. 1979. *Nuclear reactor theory*. RE Krieger Publishing Company.
- BELLMAN, R., WING, G. M., BELLMAN, R. E., AND BELLMAN, R. E. 1975. *An introduction to invariant imbedding*. SIAM.
- BEN-ARTZI, A., EGAN, K., DURAND, F., AND RAMAMOORTHI, R. 2008. A precomputed polynomial representation for interactive BRDF editing with global illumination. *ACM Trans. Graph.* 27, 2.
- BHATE, N., AND TOKUTA, A. 1992. Photorealistic volume rendering of media with directional scattering. In *Third Eurographics Workshop on Rendering*.
- BOHREN, C., AND HUFFMAN, D. 1983. *Absorption and scattering of light by small particles*. Wiley-Vch.
- BOTTOU, L., AND BOUSQUET, O. 2008. The Tradeoffs of Large Scale Learning. *NIPS*.
- CHANDRASEKHAR, S. 1960. *Radiative transfer*. Dover.
- CHEN, C., LU, J., DING, H., JACOBS, K., DU, Y., HU, X., ET AL. 2006. A primary method for determination of optical parameters of turbid samples and application to intralipid between 550 and 1630 nm. *Optics Express* 14, 16.
- DEBEVEC, P., HAWKINS, T., TCHOU, C., DUKER, H., SAROKIN, W., AND SAGAR, M. 2000. Acquiring the reflectance field of a human face. In *Proceedings of SIGGRAPH 2000, Annual Conference Series*.
- DONNER, C., AND JENSEN, H. 2005. Light diffusion in multi-layered translucent materials. *ACM Trans. Graph.* 24, 3.
- DONNER, C., WEYRICH, T., D'ÉON, E., RAMAMOORTHI, R., AND RUSINKIEWICZ, S. 2008. A layered, heterogeneous reflectance model for acquiring and rendering human skin. *ACM Trans. Graph.* 27, 5.
- DUCHI, J., SHALEV-SHWARTZ, S., SINGER, Y., AND CHANDRA, T. 2008. Efficient projections onto the  $l_1$ -ball for learning in high dimensions. *ICML*.
- DUTRÉ, P., BALA, K., AND BEKAERT, P. 2006. *Advanced global illumination*. AK Peters, Ltd.



**Figure 12:** Top: Rendering of materials in natural illumination using our acquired material parameter values. Bottom: Same image with RGB vectors normalized to unit norm, to visualize color variations.

FLEMING, R., AND BÜLTHOFF, H. 2005. Low-level image cues in the perception of translucent materials. *ACM Transactions on Applied Perception (TAP)* 2, 3.

FRISVAD, J., CHRISTENSEN, N., AND JENSEN, H. 2007. Com-

puting the scattering properties of participating media using lorenz-mie theory. *ACM Trans. Graph.* 26, 3.

FUCHS, C., CHEN, T., GOESELE, M., THEISEL, H., AND SEIDEL, H. 2007. Density estimation for dynamic volumes. *Com-*

- puters & Graphics 31, 2.
- GHOSH, A., ACHUTHA, S., HEIDRICH, W., AND O'TOOLE, M. 2007. BRDF acquisition with basis illumination. *IEEE CVPR*.
- GKIOULEKAS, I., XIAO, B., ZHAO, S., ADELSON, E., ZICKLER, T., AND BALA, K. 2013. Understanding the role of phase function in translucent appearance. *To appear in ACM Trans. Graph.* 32, 5.
- GOESELE, M., LENSCH, H., LANG, J., FUCHS, C., AND SEIDEL, H. 2004. Disco: acquisition of translucent objects. *ACM Trans. Graph.* 23, 3.
- GROEMER, H. 1996. *Geometric applications of Fourier series and spherical harmonics*. Cambridge University Press.
- GU, J., NAYAR, S., GRINSPUN, E., BELHUMEUR, P., AND RAMAMOORTHY, R. 2008. Compressive structured light for recovering inhomogeneous participating media. *ECCV*.
- GUPTA, M., AGRAWAL, A., VEERARAGHAVAN, A., AND NARASIMHAN, S. 2011. Structured light 3D scanning in the presence of global illumination. *IEEE CVPR*.
- HAN, C., SUN, B., RAMAMOORTHY, R., AND GRINSPUN, E. 2007. Frequency domain normal map filtering. *ACM Trans. Graph.* 26, 3.
- HASINOFF, S., DURAND, F., AND FREEMAN, W. 2010. Noise-optimal capture for high dynamic range photography. *IEEE CVPR*.
- HAWKINS, T., EINARSSON, P., AND DEBEVEC, P. 2005. Acquisition of time-varying participating media. *ACM Trans. Graph.* 24, 3.
- HEIKKILA, J. 2000. Geometric camera calibration using circular control points. *IEEE Transactions of Pattern Analysis and Machine Intelligence* 22, 10.
- HENYEV, L., AND GREENSTEIN, J. 1941. Diffuse radiation in the galaxy. *The Astrophysical Journal* 93.
- HOLROYD, M., AND LAWRENCE, J. 2011. An analysis of using high-frequency sinusoidal illumination to measure the 3d shape of translucent objects. *IEEE CVPR*.
- HULLIN, B., FUCHS, M., AJDIN, B., IHRKE, I., SEIDEL, H., AND LENSCH, H. 2008. Direct visualization of real-world light transport. *Vision, Modeling, and Visualization 2008*.
- ISHIMARU, A. 1978. *Wave propagation and scattering in random media*. Wiley-IEEE.
- JAKOB, W., ARBREE, A., MOON, J., BALA, K., AND MARSCHNER, S. 2010. A radiative transfer framework for rendering materials with anisotropic structure. *ACM Trans. Graph.* 29, 4.
- JENSEN, H., MARSCHNER, S., LEVOY, M., AND HANRAHAN, P. 2001. A practical model for subsurface light transport. In *Proceedings of SIGGRAPH 2001, Annual Conference Series*.
- JENSEN, H. 2001. *Realistic image synthesis using photon mapping*. AK Peters, Ltd.
- JOHNSON, C., AND GABRIEL, D. 1994. *Laser light scattering*. Dover.
- JÖRGENS, K., AND ROACH, G. 1982. *Linear integral operators*. Pitman.
- KATO, T. 1966. *Perturbation Theory for Linear Operators*. Springer.
- LAFORTUNE, E. 1996. *Mathematical models and Monte Carlo algorithms for physically based rendering*. PhD thesis, University of Leuven.
- LANG, S. 1993. *Real and functional analysis*. Springer.
- LARSEN, E. W., AND HABETLER, G. J. 1973. A functional-analytic derivation of case's full and half-range formulas. *Communications on Pure and Applied Mathematics* 26, 4.
- LAWRENCE, J., BEN-ARTZI, A., DECORO, C., MATUSIK, W., PFISTER, H., RAMAMOORTHY, R., AND RUSINKIEWICZ, S. 2006. Inverse shade trees for non-parametric material representation and editing. *ACM Trans. Graph.* 25, 3.
- LEVEQUE, R. 2007. *Finite Difference Methods for Ordinary and Partial Differential Equations, Steady-State and Time-Dependent Problems*. SIAM.
- MCCORMICK, N., AND SANCHEZ, R. 1981. Inverse problem transport calculations for anisotropic scattering coefficients. *Journal of Mathematical Physics* 22, 199.
- MUKAIGAWA, Y., YAGI, Y., AND RASKAR, R. 2010. Analysis of light transport in scattering media. *IEEE CVPR*.
- NARASIMHAN, S., GUPTA, M., DONNER, C., RAMAMOORTHY, R., NAYAR, S., AND JENSEN, H. 2006. Acquiring scattering properties of participating media by dilution. *ACM Trans. Graph.* 25, 3.
- NAYAR, S., KRISHNAN, G., GROSSBERG, M., AND RASKAR, R. 2006. Fast separation of direct and global components of a scene using high frequency illumination. *ACM Trans. Graph.* 25, 3.
- O'TOOLE, M., AND KUTULAKOS, K. N. 2010. Optical computing for fast light transport analysis. *ACM Trans. Graph.* 29, 6.
- PEERS, P., VOM BERGE, K., MATUSIK, W., RAMAMOORTHY, R., LAWRENCE, J., RUSINKIEWICZ, S., AND DUTRÉ, P. 2006. A compact factored representation of heterogeneous subsurface scattering. *ACM Trans. Graph.* 25, 3.
- PINE, D., WEITZ, D., ZHU, J., AND HERBOLZHEIMER, E. 1990. Diffusing-wave spectroscopy: dynamic light scattering in the multiple scattering limit. *Journal de Physique* 51, 18.
- PRAHL, S., VAN GEMERT, M., AND WELCH, A. 1993. Determining the optical properties of turbid media by using the adding-doubling method. *Applied optics* 32, 4.
- PUSEY, P. 1999. Suppression of multiple scattering by photon cross-correlation techniques. *Current opinion in colloid & interface science* 4, 3.
- RAMAMOORTHY, R., AND HANRAHAN, P. 2001. A signal-processing framework for inverse rendering. In *Proceedings of SIGGRAPH 2001, Annual Conference Series*.
- REYNOLDS, L., AND MCCORMICK, N. 1980. Approximate two-parameter phase function for light scattering. *JOSA* 70, 10.
- RUSHMEIER, H., AND TORRANCE, K. 1987. The zonal method for calculating light intensities in the presence of a participating medium. In *Computer Graphics*, vol. 21.
- SINGER, J., GRÜNBAUM, F., KOHN, P., ZUBELLI, J., ET AL. 1990. Image reconstruction of the interior of bodies that diffuse radiation. *Science* 248, 4958.

- SLOAN, P., KAUTZ, J., AND SNYDER, J. 2002. Precomputed radiance transfer for real-time rendering in dynamic, low-frequency lighting environments. *ACM Trans. Graph.* 21, 3.
- TONG, X., WANG, J., LIN, S., GUO, B., AND SHUM, H. 2005. Modeling and rendering of quasi-homogeneous materials. *ACM Trans. Graph.* 24, 3.
- VEACH, E. 1997. *Robust Monte Carlo methods for light transport simulation*. PhD thesis, Stanford University.
- WALTER, B., ZHAO, S., HOLZSCHUCH, N., AND BALA, K. 2009. Single scattering in refractive media with triangle mesh boundaries. *ACM Trans. Graph.* 28, 3.
- WANG, J., ZHAO, S., TONG, X., LIN, S., LIN, Z., DONG, Y., GUO, B., AND SHUM, H. 2008. Modeling and rendering of heterogeneous translucent materials using the diffusion equation. *ACM Trans. Graph.* 27, 1.
- WU, D., O'TOOLE, M., VELTEN, A., AGRAWAL, A., AND RASKAR, R. 2012. Decomposing global light transport using time of flight imaging. *IEEE CVPR*.
- WYMAN, D., PATTERSON, M., AND WILSON, B. 1989. Similarity relations for the interaction parameters in radiation transport. *Applied optics* 28, 24.
- YOSIDA, K. 1996. *Functional analysis*. Springer.